

**UTILITY
PATENT APPLICATION
TRANSMITTAL**

Attorney Docket No.

198368US17

First Inventor or Application Identifier

ALAN SHINN

Title

PYROS KINETIX READER FOR CONDUCTING ASSAYS

APPLICATION ELEMENTS

See MPEP chapter 600 concerning utility patent application contents

1. ☒ Fee Transmittal Form (e.g. PTO/SB/17)
(Submit an original and a duplicate for fee processing)

2. ☒ Specification Total Sheets **39**

3. ☒ Drawing(s) (35 U.S.C. 113) Total Sheets **23**

4. ☐ Oath or Declaration Total Pages

a. ☐ Newly executed (original or copy)

b. ☐ Copy from a prior application (37 C.F.R. §1.63(d))
(for continuation / divisional w/ box 16 completed)

i. ☐ **DELETION OF INVENTOR(S)**
Signed statement attached deleting inventor(s) named in
the prior application, see 37 C.F.R. §1.63(d)(2) and
1.33(b).

5. ☐ CD-ROM or CD-R in duplicate, large table or Computer
Program (*Appendix*)

6. ☐ Nucleotide and/or Amino Acid Sequence Submission
(if applicable, all necessary)

a. ☐ Computer Readable Form (CRF)

b. Specification or Sequence Listing on:

i. ☐ CD-ROM or CD-R (2 copies); or

ii. ☐ Paper

c. ☐ Statements verifying identity of above copies

ADDRESS TO:

Assistant Commissioner for Patents
Box Patent Application
Washington, DC 20231

ACCOMPANYING APPLICATION PARTS

7. ☐ Assignment Papers (cover sheet & document(s))

8. ☐ Application Data Sheet. See 37 CFR 1.76

9. ☐ 37 C.F.R. §3.73(b) Statement ☐ Power of Attorney
(when there is an assignee)

10. ☐ English Translation Document (if applicable)

11. ☒ Information Disclosure
Statement (IDS)/PTO-1449 ☒ Copies of IDS
Citations

12. ☐ Preliminary Amendment

13. ☒ White Advance Serial No. Postcard

14. ☐ Certified Copy of Priority Document(s)
(if foreign priority is claimed)

15. ☐ Applicant claims small entity status.
See 37 CFR 1.27

16. ☒ Other: List of Inventors' Names and Addresses
Request for Priority

16. If a CONTINUING APPLICATION, check appropriate box, and supply the requisite information below:

☐ Continuation

☐ Divisional

☐ Continuation-in-part (CIP)

of prior application no.:

Prior application information: Examiner:

Group Art Unit:

For CONTINUATION OR DIVISIONAL APPS only: The entire disclosure of the prior application, from which an oath or declaration is supplied under Box 4b, is considered a part of the accompanying continuation or divisional application and is hereby incorporated by reference. The incorporation can only be relied upon when a portion has been inadvertently omitted from the submitted application parts.

17. Amend the specification by inserting before the first line the sentence:

☐ This application is a ☐ Continuation ☐ Division ☐ Continuation-in-part (CIP)
of application Serial No. Filed on

☒ This application claims priority of provisional application Serial No. 60/167,618 Filed November 26, 1999

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IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

INVENTOR(S) ALAN SHINN, ET AL

SERIAL NO: New Application

FILING DATE: Herewith

FOR: PYROS KINETIX READER FOR CONDUCTING ASSAYS

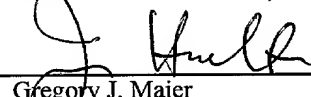
FEE TRANSMITTAL

ASSISTANT COMMISSIONER FOR PATENTS
WASHINGTON, D.C. 20231

FOR	NUMBER FILED	NUMBER EXTRA	RATE	CALCULATIONS
TOTAL CLAIMS	83 - 20 =	63	× \$18 =	\$1,134.00
INDEPENDENT CLAIMS	10 - 3 =	7	× \$80 =	\$560.00
<input type="checkbox"/> MULTIPLE DEPENDENT CLAIMS (If applicable)			+ \$270 =	\$0.00
<input checked="" type="checkbox"/> LATE FILING OF DECLARATION			+ \$130 =	\$130.00
BASIC FEE				\$710.00
TOTAL OF ABOVE CALCULATIONS				\$2,534.00
<input type="checkbox"/> REDUCTION BY 50% FOR FILING BY SMALL ENTITY				\$0.00
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<input type="checkbox"/> RECORDATION OF ASSIGNMENT			+ \$40 =	\$0.00
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- ☐ Please charge Deposit Account No. 15-0030 in the amount of _____ A duplicate copy of this sheet is enclosed.
- ☒ A check in the amount of \$2,534.00 to cover the filing fee is enclosed.
- ☒ The Commissioner is hereby authorized to charge any additional fees which may be required for the papers being filed herewith and for which no check is enclosed herewith, or credit any overpayment to Deposit Account No. 15-0030. A duplicate copy of this sheet is enclosed.

Respectfully Submitted,

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IN RE APPLICATION OF: ALAN SHINN, ET AL

FOR: PYROS KINETIX READER FOR CONDUCTING ASSAYS

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A declaration containing all the necessary information will be submitted at a later date.

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TITLE OF THE INVENTION

PYROS KINETIX READER FOR CONDUCTING ASSAYS

CROSS-REFERENCE TO RELATED APPLICATIONS

- 5 This application claims the benefit of U.S. provisional application No. 60/167,618 filed November 26, 1999.

BACKGROUND OF THE INVENTIONField of the Invention:

- 10 This invention is directed towards the Pyros Kinetix reader for conducting assays. More specifically, this invention is directed to providing an analytical device that, in one embodiment, conveniently and accurately assays both turbidity and chromogenic reactions in plural vessels.

15 Discussion of the Background:

- Optical techniques are commonly used to transduce a number of different chemical and biological parameters. Among many thousand such examples, turbidometric measurements can be used to bioassay and/or bioscreen for the presence of endotoxin using *Limulus* amebocyte lysate (LAL) such as PYROTELL-T (Associates of Cape Cod, Falmouth, MA). Similarly, chromogenic measurements can be used to bioassay and/or bioscreen for the presence of endotoxin using the POLYCHROME chromogenic formulation of LAL (Associates of Cape Cod, Falmouth, MA), which releases a yellow chromophore when exposed to endotoxin.

- Many different instruments have been described that use optical techniques to transduce these and other such biological parameters. For example, Hoyt (US 4,936,682) describes an instrument for measuring the light absorption characteristics of a plurality of samples arranged in a substantially circular pattern about a single incandescent light source. Incandescent light sources are however only suitable for performing certain types of assays since their emission intensity is primarily in the IR and long wavelength portion of the visible spectrum. Moreover, incandescent light sources require intensity adjustments to maintain a relatively constant emission flux, have limited operational lifetimes, and, as a consequence of

resistive heating of the filament, dissipate large amounts of heat that often complicate temperature control in incubators. Finally, since incandescent sources require relatively large amounts of power, they are commonly driven by high power AC sources such as line sources and microcontroller-based modulation of incandescent source intensity is relatively difficult to implement. Shirasawa (US 5,337,139) describes a multichannel optical measuring system which uses multiple branches of a quartz optical fiber to project light from mercury or xenon lamps at glass cuvettes that contain biological cell samples in order to perform fluorometric measurements. Shirasawa (US 5,337,139) also describes that a light emitting diode (LED)/photodiode pair can be associated with each glass cuvette to generate a signal related to the intensity of transmitted light through the cuvette. Mioduski (US 3,882,318) describes a reaction block configured to hold a reaction chamber where a specimen and a test reagent are mixed. The reaction block has two optical paths therethrough, one for conducting a transmittance measurement of the specimen/test reagent mixture, and the other to detect the presence of a reaction chamber within the block. Each reaction block has an associated printed circuit board for detecting light output from both paths. Noeller (US 4,784,947) describes a method for photographically recording fluorometric and nephelometric analyses performed using a photo-flash or a strobe light photon source. As both the light transduction and light generation described by Noeller (US 4,784,947) only occurs at discrete times, continuous monitoring and automated data analysis is not possible.

The disclosure of each of the above-noted patents is incorporated herein by reference.

SUMMARY OF THE INVENTION

Accordingly, one object of this invention is to provide a novel method and device for conducting assays.

Another object of this invention is to provide a novel method and device that, in one embodiment, allows a user to simultaneously assay both turbidity and chromogenic reactions in plural vessels.

Another object of this invention is to provide a novel method and device that, in one embodiment, allows a user to conduct several assays simultaneously, each assay not necessarily having a same start time.

Another object of this invention is to provide a novel method and device that, in one embodiment, reduces device component and assembly costs, minimizes the size of the device, makes repair easier.

Another object of this invention is to provide a novel method and device that, in one embodiment, allows a user to incubate plural assays in plural vessels using a minimum of power while maintaining a desired incubation temperature.

These and other objects of the invention can be realized by using a PYROS KINETIX READER and similar devices. Such devices can include, according to one embodiment, a single LED source providing illumination to plural vessels through a radial waveguide.

Some embodiments can include two LED sources in a single device, each illuminating plural vessels along a different radial waveguide. Some embodiments can include more than two LED sources in a single device. Other embodiments can include one or more radial waveguides for presenting emitted light to the plural vessels at a high intensity. Other embodiments can present emitted light along two radial waveguides through a single vessel, the first radial waveguide being used to detect a presence of the vessel and the second radial waveguide being used to transduce an optical property of an analyte within the vessel. Some embodiments include modulation of the emission intensity of the one or more LED sources, this modulation being, e.g., a step function. In some embodiments, this modulation is microprocessor-based. In other embodiments, this modulation is mechanical, analog, or otherwise electronically implemented. In some embodiments, the LED source(s) emit substantially at 470 nm +/- 30 nm. In some embodiments, one or more optical filters is placed along an optical path that passes through the vessel.

Other embodiments of such devices can include the vessels arranged in a substantially circular geometry around the LED light source(s). Other embodiments may include plural groups of two or more vessels at two or more different radii about a center. Another embodiment may include two groups of 48 vessels at two different radii about the center. In some embodiments, an LED is positioned at the center point. In some embodiments, one or more optical waveguides is used to substantially evenly distribute light from one or more LED's to several vessels. In some embodiments, a lens is used to position a virtual image of one or more LED's at the center. In some embodiments, multiple LED's are vertically staggered along a line passing through the center.

Other embodiments of such devices can include a single printed circuit board containing plural phototransducers. Some embodiments may include a single printed board having all phototransducers. Some embodiments provide plural vessels in a same plane, and a plane of such a single printed circuit board being substantially parallel to such a plane.

5 Some embodiments provide a plane of such a single printed circuit board below at least one vessel. In some embodiments, a light pipe is used to guide light transmitted along an optical path through a vessel to such a single printed circuit board.

Other embodiments of such devices can include a multicomponent support for the vessels, a first component being chosen to conduct heat for incubating one or more vessels at
10 a set temperature. In some embodiments, another component is chosen to thermally insulate the first component and reduce power demands of the device. In some embodiments, the other component is lighter than the first component and reduces the net weight of the device.

Other embodiments of such devices can include a precalibrated temperature transducer that reduces calibration demands for operating such a device.

15 The aforementioned and other objects of the invention can also be realized using methods that are simple to implement upon the PYROS KINETIX READER and other similar devices. A method for performing assays can involve generating light using a LED, radially guiding a portion of the generated light, transmitting a portion of the guided light through a plurality of vessels, and transducing a portion of the transmitted light to assay a
20 sample. In some embodiments, a portion of the generated light can be transmitted through a side or a bottom portion of the plurality of vessels and used to detect the presence of the plurality of vessels. In other embodiments, a portion of the transmitted light can be reflected using a light pipe. In some embodiments, a portion of the generated light can be diverged. In other embodiments, the generated light can be modulated to yield a background
25 measurement.

BRIEF DESCRIPTION OF THE DRAWINGS

A more complete appreciation of the invention and many of the attendant advantages thereof will be readily obtained as the same become better understood by reference to the
30 following detailed description when considered in connection with the accompanying drawings, wherein:

FIGS. 1A and 1B illustrate, respectively, a top view and a side view of an exemplary optical system according to the present invention;

FIGS. 2A, 2B, and 2C illustrate a side view of various light paths through an exemplary optical system without a sample holding vessel present, with a sample holding vessel present, and with a sample holding vessel present at an increased magnification;

FIGS. 3A and 3B illustrate, respectively, a top view and a side view of an exemplary embodiment of the optical system that includes a central light source with multiple wells;

FIGS. 4A and 4B illustrate, respectively, a top view and a side view of a second exemplary embodiment of the radial light guide **30**;

FIGS. 5A and 5B illustrate, respectively, a top view and a side view of an exemplary embodiment of the optical system that includes the second exemplary embodiment of the radial light guide **30**;

FIGS. 6A and 6B illustrate, respectively, a top view and a side view of a third exemplary embodiment of the radial light guide **30**;

FIGS. 7A and 7B illustrate, respectively, a top view and a side view of an exemplary embodiment of the optical system that includes the third exemplary embodiment of the radial light guide **30**;

FIG. 8 illustrates a schematic of a top view of an exemplary arrangement of a optical system that includes the third exemplary embodiment of the radial light guide **30**;

FIG. 9 illustrates an exemplary vessel support **80** containing two concentric circular rows of wells **45**, as well as various components to be entirely or partially inserted into the exemplary vessel support **80**;

FIG. 10 illustrates an exploded view of an assay device according to the present invention;

FIG. 11 illustrates a wireframe view of an exemplary assembled assay device;

FIG. 12 illustrates an exemplary electronics block diagram of an assay device;

FIGS. 13A-C illustrate a top view in the absence of an analyte holding vessel **40**, a top view in the presence of an analyte holding vessel **40**, and a side view in the presence of an analyte holding vessel **40** that uses an exemplary side wall tube detection scheme with a single radial light guide **30**;

FIG. 14 illustrates an exemplary process loop for monitoring and controlling the incubation temperature according to the present invention;

FIG. 15 illustrates a process flow for an exemplary on/off modulation of the light output by LED source **1** for background correction; and

FIG. 16 illustrates an exemplary computer system **801** that can form an external control/record processor in an embodiment of the present invention.

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DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring now to the drawings, wherein like reference numerals designate identical or corresponding parts throughout the several views, and more particularly to FIG. 1 thereof, which illustrates an exemplary optical system according to the present invention. The illustrated optical system generates light, radially guides it to one or more vessels containing an analyte, transmits the light through the vessel and/or the analyte, and then pipes the light to one or more light transducers where it is transduced. As used herein, radial guiding refers to the transmission of light to plural vessels along plural optical paths, wherein the transmittance along the various paths is substantially equal. This situation is possible to implement using a circular (or arcular) waveguide with a source located at the center, hence giving rise to the term “radial guiding.”

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In FIGS. 1A and 1B, LED source **1** generates and emits photons, and can also optionally serve to collimate and/or focus the generated photons. Examples of commercially available LED's that can form the LED source **1** are the Nichia P/N NSPB500S, the Kingbright P/N L934MBC, and the Hewlett-Packard P/N HLMP-CB16. LED's generate relatively large photon fluxes over relatively narrow bandwidths, especially relative to incandescent sources which emit over a very large bandwidth. In one embodiment, LED source **1** can generate photons centered around substantially 470 nm with a bandwidth +/- 30 nm, although those skilled in the art can increase or decrease the center wavelength and the bandwidth surrounding it to provide different responses. Naturally, plural LED's may be used along with multiple versions of the illustrated optical system in the same assay device. In such a case, LED's with different center wavelengths and/or intensities may be selected to, e.g., provide broader dynamic range for assays, allow dual wavelength assays to, e.g., increase sensitivity and/or allow a user to use plural chromophores and/or obtain better background correction information.

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Also illustrated in FIG. 1B is an optical filter **2** between the LED source **1** and the radial waveguide **30**. The filter **2** is optional; since a LED emission spectrum is already

relatively narrowband, it is often not necessary to include filter 2, which further lowers the cost and power requirements of the optical system. However, in some applications that have precise wavelength requirements, such as spectroscopic analyses or chromogenic assays of complex samples, a filter 2 may be desirable.

5 In the illustrated embodiment, light emitted by LED source 1 is guided radially by a radial light guide 30 that includes a light coupling total internal reflection (TIR) cone 35 for coupling the emitted light into the radial light guide 30. As illustrated, light coupling TIR cone 35 is centered within the radial light guide 30 and substantially above the LED source 1. In such a geometry, light emitted by LED source 1 is substantially evenly transmitted from the center of light guide 20 toward the perimeter of radial light guide 30. Radial light guide 30 can be formed of, e.g., acrylic cast into a mold that forms light coupling TIR cone 35. The radial light guide 30 with a light coupling TIR cone 35 allows a 20 to 100 mW LED source 1 to provide as much illumination to the analyte holding vessel 40 as a 20 W incandescent bulb.

15 A single well 45 configured to support an analyte holding vessel 40 is illustrated beyond the perimeter of the radial light guide 30. Naturally, it is both possible and desirable to use plural wells 45 and analyte holding vessels 40 (not shown). The distribution of such wells 45 relative to the radial light guide 30 will be discussed further in, e.g., FIGS. 3 and 11. The illustrated well 45 is configured to support an analyte holding vessel 40 that is a test tube, although other suitable vessels, such as optical cuvettes and capillaries, may be used. It is only important that analyte holding vessel 40 be sufficiently transparent over the emission spectrum of LED source 1 to perform the desired assay.

20 The exemplary optical system of FIG. 2 also includes a pair of light pipes 60 and 70 along a pair of paths that join the real or virtual position of the LED source 1 and some point in or on an analyte holding vessel 40 in the well 45. The pair of light pipes 60 and 70 neighbor the well 45. Light transmitted through the well 45 is incident upon the pair of light pipes 60 and 70 (provided no analyte holding vessel 40 is present), and reflected in a direction determined by the orientation of a total internal reflection (TIR) surface 21. The pair of light pipes 60 and 70 thus allow an optical transducer to be located away from a straight line path that join the real or virtual position of the LED source 1 and some point in or on the analyte holding vessel 40 in the well 45. This is desirable in the interest of simplifying device design, limiting the number of harness connections, decreasing the cost of

the device, and simplifying maintenance and repair. As illustrated, the light receiving portion of light pipe **60** is located along a path that joins the real or virtual position of the LED source **1** and a point on the bottom curvature of an analyte holding vessel **40** positioned in the well **45**. When an analyte holding vessel **40** is present in well **45**, light passing along this line through the radial light guide **30** is significantly deflected out of this path due to refraction by the analyte holding vessel **40**, and a light transducer **65** located at the output of light pipe **60** can easily detect the insertion and/or removal of analyte holding vessel **40** by monitoring the intensity of the received light. Absorption and/or reflection of the light that passes along this path can also decrease the intensity of the received light and detect the presence of an analyte holding vessel **40** in well **45**. Alternatively, the light receiving portion of light pipe **60** can be located along a path that joins the real or virtual position of the LED source **1** and a point on the side curvature of the analyte holding vessel **40** to obtain a similar sensitivity, as further illustrated in FIGS. 13A-C.

Light pipe **70**, on the other hand, is preferably located along a light path that joins the real or virtual position of the LED source **1** and a point near the center of an inserted analyte holding vessel **40**, but away from the bottom. As such, a relatively long pathlength through the analyte holding vessel **40** is examined and refraction (due to, e.g., tubular analyte holding vessels **40**) is minimized.

In the illustrated embodiment of FIG. 1B, both light pipes **60** and **70** receive light from a same radial light guide **30**. This is not necessarily the case. For example, two different radial light guides **20** can each transmit light to a single respective light pipe **60** and **70**. Moreover, in the case of plural test wavelengths, even three or more different radial light guides **20** can be used with associated light pipes.

In the illustrated embodiment, both TIR surfaces **21** reflect light downward, substantially at right angles relative to the respective path of that light through the analyte holding vessel **40**. This is preferred, since no tilting and/or stoppering of the analyte holding vessel **40** is required and the light transducers **65** and **75** for multiple analyte holding vessels **40** can be positioned in a single printed circuit board located below and substantially parallel with the radial light guide **30**. Naturally, in some embodiments of the invention, the TIR surfaces **21** and pair of light pipes **60** and **70** can be eliminated in whole or in part, although this will often require the placement of the light transducers **65** and **75** for multiple analyte holding vessels **40** upon multiple printed circuit boards. At the output of the pair of light

pipes **60** and **70**, a pair of light transducers **65** and **75** can be used to determine the transmissivity of both optical paths. Suitable, commercially available light transducers **65** and **75** include photodiodes such as the Centrovision P/N BPW-34, Hamamatsu P/N S4707-01, Hamamatsu P/N S3407-01, UDT Sensors P/N BPW34, UDT Sensors P/N BPW34B, Infinition P/N BPW34, Infinition P/N BPW34 B, and the Perkin Elmer P/N VTD34.

A further illustration of side views of various light paths **100**, **101**, and **102** through an exemplary optical system with and without a sample holding vessel present is provided in FIGS. 2A, 2B, and 2C (albeit at higher magnification). In FIG. 2A, photons generated at the LED source **1** are reflected by the light coupling TIR cone **35** and carried along radial light guide **30** to a vessel support **80** that may or may not support an analyte holding vessel **40** therein. If an analyte holding vessel **40** is not supported by the a particular well **45** of the vessel support **80**, then the light path **101** will conduct a relatively high intensity of light to light pipe **60**, which in turn conducts the light to light transducer **65**. On the other hand, if a (filled) analyte holding vessel **40** is supported by a particular well **45** of the vessel support **80**, then light originally on light path **101** is deflected along light path **102**, and a relatively low intensity of light is received at light pipe **60** and light transducer **65**. Thus, by measuring an intensity of the light received at light transducer **65**, the presence of an analyte holding vessel **40** in a well **45** of the vessel support **80** can be made.

FIG. 2C illustrates a side view of various light paths through an exemplary optical system with a sample holding vessel present at an increased magnification. As illustrated, light that has passed through the radial light guide **30** is directed downward due to refraction caused by the base of an analyte holding vessel **40** in a well **45** of the vessel support **80**. Refraction need not be the physical origin of the decreased light intensity received at light guide **60**. For example, reflection and/or absorption can also cause reduced light transmission to light guide **60**.

As illustrated in FIGS. 2A, 2B, and 2C, since light path **100** is incident upon a position substantially at the middle of analyte holding vessel **40**, the direction of light path **100** remains substantially unchanged by the presence of analyte holding vessel **40**. Naturally, the intensity of light transmitted along light path **100** will change, and this intensity change will be used to assay the contents of analyte holding vessel **40**.

Also illustrated in FIG. 2A and 2B is a positioning sleeve **11** arranged about the LED source **1**. The positioning sleeve **11** serves to accurately center LED source **1** directly under

light coupling TIR cone 35, ensuring substantially uniform radial illumination by light guided through radial light guide 30.

FIGS. 3A and 3B illustrate, respectively, a top view and a side view of an exemplary embodiment of the optical system that includes a central light source with multiple wells 45 of the vessel support 80 for holding multiple analyte holding vessels 40. In the illustrated embodiment, the multiple wells 45 are arranged radially about the light coupling TIR cone 35 of the radial light guide 30. As such, the multiple wells 45 of the vessel support 80 receive substantially equal radiant fluxes from the LED source 1. Moreover, if the vessel support 80 is radially symmetric, this radial symmetry can be exploited to maintain all wells 45 of the vessel support 80 at a substantially equal temperature. For example, if the vessel support 80 includes a ring made of a thermally conducting material (e.g., a metal such as aluminum or copper such as heat conducting block 85 shown in e.g., FIG. 10), then a heater ring (such as heater 90 shown in e.g., FIG. 10) can be disposed just inside and/or outside of the vessel support 80 and all wells 45 of the vessel support 80 will be maintained at a substantially equal temperature. Thus, even if the absolute incubation temperature is subject to errors due to, e.g., thermal fluctuations and/or miscalibrated equipment, then accurate differential measurements across samples within different wells 45 of the vessel support 80 will still be possible. Both the heating of and disposition of wells 45 within the vessel support 80 will be discussed in more detail in regard to FIG. 9.

FIGS. 4A and 4B illustrate, respectively, a top view and a side view of a second exemplary embodiment of the radial light guide 30, namely a curved wedge lightguide. As with the radial light guide 30 of FIGS. 1A and 1B, the radial light guide 30 of FIGS. 4A and 4B guides light emitted by LED source 1 (optionally passing through a light filter 2) radially to multiple wells 45 within the vessel support 80. With curved wedge waveguides, plural LED sources can be vertically staggered, and the light illuminating the analyte holding vessels 40 in wells 45 appear to originate from a single, central source 111. The radial light guide 30 of FIGS. 4A and 4B is particularly useful for several different reasons. For example, by reducing the total number of wells 45 that are illuminated by a particular LED source 1, then the intensity per well 45 is increased. This effect can be augmented by collecting and/or focusing light upon the end of radial light guide 30 using, e.g., lenses and spherical and/or parabolic reflectors (not shown). The increased light intensity per well 45 is particularly useful when, e.g., assaying samples with a low transmittance. Another reason

that the radial light guide 30 of FIGS. 4A and 4B is particularly useful is that several such light guides and LED sources 1 may be used in a single device for conducting assays. This broadens the range of available assays that may be performed upon the analyte holding vessels 40 in vessel support 80. For example, some wells 45 of the vessel support 80 may be dedicated to assaying for one chromophore, while other wells 45 may be dedicated to assaying for another chromophore that has a different absorption spectrum. Since different LED sources 1 can be used to sample separate groups of wells 45, each chromophore can be probed at a wavelength for which it has a near-maximum response (e.g., absorbance), and an increased sensitivity to each chromophore can be achieved. Moreover, different filters can be inserted between each of the LED sources 1 and the radial light guides 30.

FIGS. 5A and 5B illustrate, respectively, a top view and a side view of an exemplary embodiment of the optical system that includes the second exemplary embodiment of the radial light guide 30. Plural LED sources 1 are available in this optical system, and light emitted by these LED sources 1 is substantially evenly distributed along the perimeter of radial light guide 30 due to the symmetric arrangement of plural versions of the second exemplary embodiment of the radial light guide 30 about a central axis. As described before, the plural LED sources 1 can have similar or different emission spectra, as desired.

FIGS. 6A and 6B illustrate, respectively, a top view and a side view of a third exemplary embodiment of the radial light guide 30, namely a lensmatic wedge lightguide. As with the radial light guide 30 of FIGS. 1A and 1B, the radial light guide 30 of FIGS. 6A and 6B guides light emitted by LED source 1 (optionally passing through a light filter 2) radially to multiple wells 45 within the vessel support 80. However, the lensmatic wedge lightguide has at least one of the light coupling face 32 (where light is received from the LED source 1) and a light decoupling face 31 (where light is transmitted to the analyte holding vessels 40 in wells 45) with a radius of curvature that is smaller than the radius of the one or more concentric rows of wells 45 in the vessel support 80 for the analyte holding vessels 40. The lensmatic wedge lightguide version of the radial light guide 30 thus can be designed to create a virtual image 111 of the LED source 1 directly at the center point of the radius of one or more concentric rows of wells 45 in the vessel support 80. Once again, substantially even radial distribution of light emitted by plural LED sources 1 can be assured, even though these sources do not occupy the same physical space.

The third embodiment (lensmatic wedge) radial light guide 30 of FIGS. 6A and 6B is

particularly useful for reasons similar to those described in regard to the second embodiment (curved wedge) of the radial light guide **30** of FIGS. 4A and 4B. For example, by reducing the total number of analyte holding vessels **40** that are illuminated by a particular LED source **1**, then the intensity per analyte holding vessel **40** is increased. This effect can be augmented by collecting and/or focusing light upon the end of radial light guide **30** using, e.g., lenses and spherical and/or parabolic reflectors (not shown). The increased light intensity per analyte holding vessel **40** is particularly useful when, e.g., assaying samples with a low transmittance. Another reason that the third embodiment (lensmatic wedge) radial light guide **30** of FIGS. 6A and 6B is particularly useful is that several such lightguides and LED sources **1** may be used in a single device for conducting assays. This broadens the range of available assays that may be performed upon the analyte holding vessels **40** in vessel support **80**. For example, some wells **45** of the vessel support **80** may be dedicated to assaying for one chromophore, while other wells **45** may be dedicated to assaying for another chromophore that has a different absorption spectrum. Since different LED sources **1** can be used to sample separate groups of wells **45**, each chromophore can be probed at a wavelength for which it has a maximum absorbance, and an increased sensitivity to each chromophore can be achieved. Moreover, different filters can be inserted between each of the LED sources **1** and the radial light guides **30**.

In contrast with the second embodiment (curved wedge) radial light guide **30** of FIGS. 4A and 4B, multiple copies of the third embodiment (lensmatic wedge) radial light guides **20** of FIGS. 6A and 6B can be maintained in a substantially single plane. As such, it is easier to stack multiple layers of the third embodiment (lensmatic wedge) radial light guides **20** so that each well **45** in vessel support **80** can be assayed by a user-selected wavelength independent of the location of well **45**. A single well **45** may also be assayed at multiple wavelengths using this approach by, e.g, multiplexing the transmission wavelength through a single well **45** by shifting the phase of an on/off modulation for different LED sources **1** stacked atop one another but illuminating a single well **45**. The stacking of multiple layers of the third embodiment (lensmatic wedge) radial light guides **20** can be accompanied by the addition of further light pipe(s) and transducer(s) (sensitive to the wavelength(s) of the further LED sources **1**) so that complete additional, independent, optical channels can be formed. Finally, lensmatic wedge radial light guides **20** are relatively easy to make.

FIGS. 7A and 7B illustrate, respectively, a top view and a side view of an exemplary embodiment of an optical system that includes the third exemplary embodiment of the radial light guide **30**, namely the lensmatic wedge. Similarly to FIGS. 5A and 5B, plural LED sources **1** are available in this optical system, and light emitted by these LED sources **1** is substantially evenly distributed along the perimeter of radial light guide **30** due to the symmetric arrangement of plural versions of the third exemplary embodiment of the radial light guide **30** about a central axis. As described before, the plural LED sources **1** can have similar or different emission spectra, as desired.

FIG. 8 illustrates a schematic of a top view of an exemplary arrangement of a optical system that includes the third exemplary embodiment of the radial light guide **30**, namely the lensmatic wedge. This is presented to emphasize that, in this case, all radial light guides **20** can form a virtual image **111** of a respective LED source **1** at a point central to all wells **45** of the vessel support **80**.

FIG. 9 illustrates an exemplary heat conducting block **85** from a vessel support **80** that contains two concentric circular rows of wells **45**. Also shown are a heater ring **90**, a temperature transducing thermistor **1000**, a fixing dowel pin **6**, O-rings **41**, and dual light pipes **675**. The heat conducting block **85** contains two concentric circular rows of wells **45** configured to support an inserted analyte holding vessel **40** (not shown). By using two concentric circular rows of wells **45**, the capacity of the instrument (i.e., number of wells **45**) can be increased. This allows for the parallel assaying of multiple analyte holding vessels **40** without an unwieldy increase in the dimensions of the vessel support **80**. In one embodiment, there are 96 wells **45** within a single vessel support **80**, distributed in two concentric circular rows.

In the illustrated embodiment, the wells **45** are relatively deep and a significant portion of an inserted analyte holding vessel **40** can be enclosed within each well **45**. Thus, cross bores (not shown) directed radially through the vessel support **80** are necessary to allow the transmission of light through the vessel support **80** to the wells **45** and light pipes **60** and **70**.

The exemplary vessel support **80** also includes a heater ring **90** that surrounds the heat conducting block **85**. By maintaining radial symmetry about a central axis for both the heater ring **90** and the wells **45** in the heat conducting block **85**, a relatively equal temperature can be maintained at each well **45** in a single row. As such, even if absolute

temperature control is ineffective, accurate differential measurements across analyte holding vessels **40** incubated in a same row can be made. In one embodiment, heater ring **90** is formed from a low power, DC heater. The power supply for such a heater ring **90** can be placed under microprocessor control and, given that the supply is DC, a source of AC electrical noise within the device for assays is eliminated.

The exemplary vessel support **80** also includes a temperature transducing thermistor **1000** that is favorably disposed in contact with or within the heat conducting block **85**. The temperature transducing thermistor **1000** can be used to generate a control signal used for the closed loop control of the temperature of heat conducting block **85**. A suitable, commercially available thermistor **1000** is the P/N QT06002-128 REV A from Quality Thermistor, Inc. For example, if the temperature transducing thermistor **1000** indicates that the temperature of the heat conducting block **85** has dropped below a predetermined (and possibly operator-set) temperature, then increased power can be presented to heater ring **90**, and the temperature of the heat conducting block **85** increased. In some embodiments of the device, assay incubation temperature is maintained at $37^{\circ} \pm 0.1^{\circ}\text{C}$ using a calibrated thermistor with a $\pm 0.1^{\circ}\text{C}$ accuracy. The look-up table for the temperature transducing thermistor **1000** is stored in a memory, and the temperature transducing thermistor **1000** is read every 3 seconds via a 12 bit A/D converter. This digital signal corresponds to the control signal for the feedback loop, and a microcontroller increases power applied to the heater when the apparent temperature drops below 36.9°C and decreases applied power when the apparent temperature exceeds 37.1°C .

The exemplary vessel support **80** can also include an O-ring **41** that can be sandwiched in each well **45**. An O-ring **41** so disposed along the interior of well **45** provides enough resistance to falling such that an analyte holding vessels **40** that is placed into a well **45** will not drop and splash the analyte. Moreover, such O-rings **41** are inexpensive and replaceable.

The exemplary vessel support **80** can also include an dual light pipe **675** that includes each of light pipes **60** and **70** inserted into the base of heat conducting block **85**. Dual light pipe **675** can be used to maintain a constant spatial relationship between each of light pipes **60** and **70**.

Finally, the exemplary vessel support **80** can also include a fixing dowel pin **6** that can be inserted into heat conducting block **85** used to fix the relative angular position of the

heat conducting block **85** relative to any support or cover therefor.

FIG. 10 illustrates the assembly of an assay device according to the present invention. The device for assays is enclosed within a base **200** and a cover **800** that protect the optical and electronic components from, e.g., dust, water splashes, and other environmental hazards.

5 In the illustrated embodiment, all light transducers **65** and **75** are arranged on a single printed circuit board assembly **300** to receive light output from a respective light pipe **60** or **70**.

Some or all electronic signal processing elements can be located on a single printed circuit board assembly **300**, such as, e.g., timing elements, A/D converters, channel multiplexers, electrical filters, switches, and/or buffers. Either a raw or a processed (e.g., sampled and
10 filtered) output from the individual light transducers **65** and **75** can be relayed to an external control/record processor by way of a multi-pin bulkhead connector (not shown) affixed to, e.g., the side wall of base **200**. Naturally, plural printed circuit board assemblies **300** can be used in some embodiments of the invention.

Depending upon the thickness of heat conducting block **85**, one or more LED
15 source(s) **1** and radial waveguide(s) **30** can be disposed substantially concentrically within heater **90** and heat conducting block **85**. If heat conducting block **85** is relatively thick, then one or more of the light paths **100** and **101** can pass through heat conducting block **85**. This can be accomplished by boring radial holes to transmit the light emitted from radial waveguide(s) **30** through an analyte holding vessel **40** in a well **45** to a respective light pipe
20 **60** or **70** which is affixed within heat conducting block **85**. The respective light pipe **60** or **70**, which can be fixed within a hole bored into the heat conducting block **85** in an axial direction, can then transmit the light to the respective light transducer **65** or **75** on printed circuit board assembly **300**. As mentioned before, if further optical channels capable of making measurements upon a single analyte holding vessel **40** in a well **45** are added, then
25 additional light pipes and light transducers can be added, as needed.

The illustrated device for assay has two separate radial waveguides **30** according to the first described embodiment, one which transmits light along light path **100** for assaying and one which transmits light along light path **101** for detecting an analyte holding vessel **40**. Naturally, other numbers and types of radial waveguides **30** are available under the current
30 invention. Moreover, one or more radial waveguide(s) **30** can be disposed such that they transmit light above heat conducting block **85** to a respective light pipe **60** or **70**, which may or may not be affixed within the heat conducting block **85**. In such a case, it may be

desirable to optically isolate the individual analyte holding vessels **40** by interposing an opaque sheet between neighboring analyte holding vessels **40**.

The two separate radial waveguides **30** are themselves optically isolated from one another through an optical separator **400**. Such an optical separator can be formed, e.g., from a thin metallic or polymeric piece that is substantially opaque in the wavelengths used by the respective one or more LED source(s) **1**.

In the illustrated embodiment, an insulating shell **500** is disposed and affixed atop the heat conducting block **85** and/or heater **90** to form vessel support **80**. The insulating shell **500** can serve multiple purposes. Firstly, by thermally isolating the heat conducting block **85** and/or heater **90**, the power requirements of the heater **90** can be reduced, and more uniform heating across the heat conducting block **85** can be obtained. Furthermore, even if insulating shell **500** were in physical contact with base **200**, then conductive thermal transport to base **200** can be minimized. Moreover, since the insulating shell **500** reduces the power requirements of heater **90** for maintaining a substantially constant incubation temperature, a DC heater **90** can be used, which is easily amenable to microprocessor-based control and eliminates background electrical noise by removing a high power AC component from the assay device. This is particularly beneficial when a printed circuit board assembly **300** contains some and/or all of the processing equipment, since the base **200** and a cover **800** can form, in some embodiments, a Faraday cage with only DC power feed lines for the internal electronic circuitry.

Another advantage of the insulating shell **500** is that it allows for the minimization of the thickness of the conducting block **85** within the vessel support **80**, and hence reduces the total weight of the instrument. For example, the insulating shell **500** can have a top face that is displaced from the conducting block **85** and holes (not shown) that support the analyte holding vessels **40** can be drilled through this top face. Thus, an analyte holding vessel **40** that is inserted into a well **45** is supported both at the conducting block **85** and at the insulating shell **500**. The use of an insulating shell thus allows for the minimization of the thickness of conducting block **85** in the vessel support **80** while maintaining support for an analyte holding vessels **40** with a minimal increase in weight, since insulating shell **500** can be made from, e.g., a polymer. An example material for the insulating shell **500** is DELRIN (acetal).

Yet another advantage of the insulating shell **500** is that it can serve to fix the position

of other components, including the O-rings **41** and the radial light guide(s) **20**, relative to the conducting block **85** and wells **45**.

In the embodiment illustrated in FIG. 10, an indicator assembly layer including a cover **700** and an LED indicator assembly **600** is included between the insulating shell **500** and the cover **800**. Both the cover **700** and LED indicator assembly **600** can be used to provide a human operator with information regarding the wells **45**. For example, an alphanumeric denominator for each well **45** can be included upon the cover **700** and the LED indicator assembly **600** can be used, e.g., to indicate to an operator that the assay device considers that an analyte holding vessel **40** has been inserted into a particular well **45**. Thus, operator error due to incomplete and/or incorrect insertion of an analyte holding vessel **40** can be avoided.

FIG. 11 illustrates a wireframe view of an exemplary 96 well assembled assay device. The 96 wells in the illustrated exemplary device are arranged in two concentric circular rows about a center point which contains a real or virtual LED source **1**. The locations of the wells **45** along the two rows are furthermore offset with regard to one another, so that a clear optical path to the outer wells from the real or virtual LED source **1** exists. Finally, there need not be any moving parts in the assay device, and moreover the entire device can be microprocessor controlled and DC powered.

FIG. 12 illustrates an exemplary electronics block diagram of an assay device. As mentioned before, a single control/record processor **610** can be used to control operation of the elements of the assay device, as well as to record the results of the assays. For example, the resistance of thermistor **1000** can be measured by, e.g., placing thermistor **1000** in a bridge and digitizing a differential voltage across the bridge using an A/D convertor **660**. The digitized differential voltage can be relayed to the control/record processor **610** which might have access to, e.g., a look-up table that associates certain differential voltages with certain temperatures. An exemplary commercially available control/record processor **610** is the Motorola P/N MC68HC711E9FN3. The control/record processor **610** can then compare the digitized differential voltage with a reference value, and increase and/or decrease the power output to heater **90** as needed. This will be discussed in more detail in regard to FIG. 14.

Another method of determining a temperature is through the use of a manufacturer-calibrated thermistor **1000**. An R-T look-up table is provided by the manufacturer for such

devices. In this case, the A/D converter **660** measures an absolute potential drop and hence resistance across the thermistor **1000**.

Another function of the control/record processor **610** is implemented using a digital connection to an LED source **1** intensity controller **650**. This intensity controller **650** can receive digital intensity control signals from the control/record processor **610** and use them to increase and/or decrease the bias voltage applied to one or more of the LED sources **1**. This will be done, e.g., when an analyte holding vessel **40** is newly inserted into a particular well **45**, or when the light received by a light transducer **75** is too low in intensity for an accurate measurement to be made by a light transducer **75**. The intensity controller **650** can also be used to modulate the bias voltage applied to the LED sources **1** as needed.

In order for the applied bias voltage to effect a light emission from the LED sources **1**, a suitable voltage across the LED sources **1** must exist (i.e., the LED sources **1** must be forward biased). This too can be determined by the control/record processor **610**, which uses a light source multiplexer **655** to selectively complete a return electrical current path through one or more particular LED sources **1**. The light source multiplexer **655** can selectively forward bias an LED source **1** in response to, e.g., the insertion of an analyte holding vessel **40** into a particular well **45** serviced by an LED source **1**, the selection of a certain assay wavelength by an operator corresponding to the emission of LED source **1**, or simply to effect an on/off modulation as described in more detail in FIG. 15.

A separate vessel detect light source **1** is illustrated in FIG. 12 for the sake of illustrating separate control of the vessel detect optical path when a dedicated radial light guide **30** is used to form light path **101**. This vessel detect light source **1** can also be formed by an LED and controlled using a light source multiplexer **655** and intensity controller **650** as described above.

Another way that the control/record processor **610** can respond to light transducer **75** receiving an insufficient light intensity is by changing an amplification gain for an amplifier associated with one or more light transducer(s) **75**. This can be done by transmitting a well select signal to well selection unit **620** along with a digital gain adjust signal to the gain adjuster **635**, which in turn can increase the gain of signal amplifier **645** for the selected well **45**. The well selection unit **620** can be formed of another multiplexer that selects the output of a particular well **45** for input to the signal amplifier **645**. Naturally, plural well selection units **620**, signal amplifiers **645**, and gain adjusters **635** can be used as well to produce a

similar action.

A similar process can be used to adjust a light intensity cut-off level for determining when an analyte holding vessel **40** is present in one or more wells **45**. Digital level adjuster **630** can be used to set an appropriate voltage for the vessel detect comparator **640** that is midway between the output voltage of light transducer **65** when an analyte holding vessel **40** is present and the output voltage of light transducer **65** when an analyte holding vessel **40** is absent from a well **45**. A voltage set signal can be transmitted from control/record processor **610** to digital level adjuster **630** at the same time that the appropriate well is identified to well selection unit **620**. Once again, plural well selection units **620**, level adjusters **630**, and vessel detect comparators **640** can be used as well to produce a similar action.

The control/record processor **610** can also be used to generate a ready signal, and error signal, and/or other indicator signals for output to indicator **11**. The indicator **11** thus serves to provide operation information to an operator.

The control/record processor **610** can also be used to handle communications with another control/record processor **610**, an output and/or input device, and/or with one or more computer-readable memory devices by way of a communications port **670**. These functions will be discussed further in regard to FIG. 16.

FIGS. 13A-C illustrate a top view in the absence of an analyte holding vessel **40**, a top view in the presence of an analyte holding vessel **40**, and a side view in the presence of an analyte holding vessel **40** that uses an exemplary side wall tube detection scheme with a single radial light guide **30**. In the illustrated example, both the light paths **100** and **101** (as well as **102**) pass through a single radial light guide **30** with the light path **101** simply being displaced by some angle from light path **100** within the single radial light guide **30**. As illustrated, the side wall of the analyte holding vessel **40** deflects the path of light that travels down light path **101** without the analyte holding vessel **40** present in the well **45** to the light path **102** when the analyte holding vessel **40** is present in the well **45**. This configuration is particularly advantageous when a flat-bottomed analyte holding vessel **40** as illustrated in FIG. 13C is used.

Furthermore, the side wall detection scheme illustrated in FIGS. 13A-C provides two further advantages. When the analyte holding vessel **40** is a test tube, the side wall curvature is often manufactured to tighter tolerances than the radius of the bottom of these vessels. As such, more reliable detection of these vessels can be obtained. Furthermore, regardless of the

type of analyte holding vessel **40**, sidewall detection allows the minimization of the length of light path **100**. Since light pipe **70** can be brought closer to the well **45**, the length of the light path **100** can be decreased, and the intensity of the light received by light pipe **70** increased.

FIG. 14 illustrates an exemplary process loop for monitoring and controlling the incubation temperature according to the present invention. In one embodiment, this process loop is performed at all times during operation of the assay device. In other words, an analyte holding vessel **40** need not be inserted into a well **45**. In step **1210**, the temperature is read using temperature transducing thermistor **1000** which can be precalibrated with corresponding temperature and resistances stored in a look-up table in computer-readable memory. Alternatively, temperature transducing thermistor **1000** can be linearized over a temperature range near a common incubation temperature such as 37.0°C. In either case, once a temperature (and/or corresponding resistance) has been determined, it is recorded in step **1220**. This can be done by writing to a computer readable memory, such as the illustrated Pyros data block **1000**. Recordation of the temperature in step **1220** need not always be performed. For example, in the case of a long assay time, only one in a certain number of measured temperatures need be recorded. Alternatively, if no analyte holding vessels **40** are located in a well **45**, then temperature need not be recorded.

In step **1230**, a determination is made as to whether the temperature read in step **1210** is within a certain range. In the illustrated process loop, if the read temperature is less than 37.1°C and greater than 36.9°C, then the process flow returns to step **1210**, perhaps after a suitable delay. However, if the read temperature is less than 36.9°C, then the process flow proceeds to step **1280**, where the heater control indicates that the power to the heater **90** should be increased. In step **1285**, another determination is made as to whether the temperature read in step **1210** falls within a certain range. The determination in step **1285** is made to determine whether a critical temperature situation due to underheating exists. For example, if the read temperature is less than 36.5°C, then a critical situation is indicated to the operator by setting a front panel LED indicator to red in step **1295**. The assay device also sets an internal status indicator to a value, e.g., 0, that indicates the presence of a critical temperature situation due to underheating. After the critical temperature situation is indicated to both the user and/or other portions of the device, both the temperature and status is recorded in step **1270** by writing to, e.g., the illustrated Pyros data block **1000**. After recordation of the temperature and status, the process flow loops back to step **1210**.

In step **1235**, if it is determined that a critical temperature situation does not exist, then the process flow proceeds to step **1270** without indicating a critical temperature situation to the user and/or other portions of the device. Once again, both the temperature and status can be recorded in step **1270** as needed by writing to, e.g., the illustrated Pyros data block **1000**. After recordation of the temperature and status, the process flow loops back to step **1210**.

In step **1230**, if the read temperature is greater than 37.1 °C, then the process flow proceeds to step **1240**, where the heater control indicates that the power to the heater **90** should be decreased and/or cut off. In step **1250**, another determination is made as to whether the temperature read in step **1210** falls within a certain range. The determination in step **1250** is made to determine whether a critical temperature situation due to overheating exists. For example, if the read temperature is greater than 37.5 °C, then a critical situation is indicated to the operator by setting a front panel LED indicator to red in step **1260**. The assay device also sets an internal status indicator to a value, e.g., 2, that indicates the presence of a critical temperature situation due to overheating. After the critical temperature situation is indicated to both the user and/or other portions of the device, both the temperature and status can be recorded in step **1270** by writing to, e.g., the illustrated Pyros data block **1000**. After recordation of the temperature and status, the process flow loops back to step **1210**.

In step **1250**, if it is determined that a critical temperature situation does not exist, then the process flow proceeds to step **1270** without indicating a critical temperature situation to the user and/or other portions of the device. Once again, both the temperature and status can be recorded in step **1270** by writing to, e.g., the illustrated Pyros data block **1000**. After recordation of the temperature and status, the process flow loops back to step **1210**.

FIG. 15 illustrates a process flow for an exemplary on/off modulation of the light output by LED source **1** for background correction. In the on/off modulation, a background light level is first determined for a particular light transducer, and then a transmitted light measurement is performed. The background level can thus be subtracted out, and more accurate measurements made. In step **1300**, a LED source **1** that provides the majority of the illumination for a particular well **45** is shut off. In a preferred embodiment, a particular well **45** already has an analyte holding vessel **40** inserted therein. The particular well **45** can be operator-identified, or the instrument can constantly cycle around all available (e.g., filled)

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FIG. 16 illustrates a computer system **801** that can form an external control/record processor in an embodiment of the present invention. For example, computer system **801** can communicate with control/record processor **610** of FIG. 12 by way of communications port **670**.

Computer system **801** includes a bus **802** or other communication mechanism for communicating information, and a processor **803** coupled with bus **802** for processing the information. Computer system **801** also includes a main memory **804**, such as a random access memory (RAM) or other dynamic storage device (e.g., dynamic RAM (DRAM), static RAM (SRAM), synchronous DRAM (SDRAM), flash RAM), coupled to bus **802** for storing information and instructions to be executed by processor **803**. In addition, main memory **804** may be used for storing temporary variables or other intermediate information during execution of instructions to be executed by processor **803**. Computer system **801** further includes a read only memory (ROM) **805** or other static storage device (e.g., programmable ROM (PROM), erasable PROM (EPROM), and electrically erasable PROM (EEPROM)) coupled to bus **802** for storing static information and instructions for processor **803**. A storage device **807** and/or **808**, such as a magnetic disk or optical disk, is provided and coupled to bus **802** by way of a disk controller **806** for storing information and instructions. Storage device **807** and/or **808** can contain the tables that record operating and/or measurement information, such as the Pyros data block **1000** of FIG. 14.

The computer system **801** may also include special purpose logic devices (e.g., application specific integrated circuits (ASICs)) or configurable logic devices (e.g., generic array of logic (GAL) or reprogrammable field programmable gate arrays (FPGAs)). Other removable media devices (e.g., a compact disc, flash memory cards, a tape, and a removable magneto-optical media) or further fixed, high density media drives, may be added to the computer system **801** using an appropriate device bus (e.g., a small computer system interface (SCSI) bus, an enhanced integrated device electronics (IDE) bus, or an ultra-direct memory access (DMA) bus). Such removable media devices and fixed, high density media drives can also contain the tables that record operating and/or measurement information, such as the Pyros data block **1000** of FIG. 14. The computer system **801** may additionally include a compact disc reader, a compact disc reader-writer unit, or a compact disc juke box,

each of which may be connected to the same device bus or another device bus.

Computer system **801** may be coupled via bus **802** to a display **810**, such as a cathode ray tube (CRT), for displaying information to a computer user. Display **810** can perform the functions of an indicator **11** as seen in FIG. 12, especially when the assay device is operated remotely from the computer system **801**. The display **810** may be controlled by a display or graphics card. The computer system includes input devices, such as a keyboard **811** and a pointing device **812** (e.g., a cursor control), for communicating information and command selections to processor **803**. The pointing device **812** (e.g., cursor control), for example, is a mouse, a trackball, or cursor direction keys for communicating direction information and command selections to processor **803** and for controlling cursor movement on the display **810**.

The computer system **801** can perform a portion or all of the processing steps of the invention in response to processor **803** executing one or more sequences of one or more instructions contained in a memory, such as the main hard disk memory **807**. Such instructions may be read into the main hard disk memory **807** from another computer readable medium, such as storage device **808**. One or more processors in a multi-processing arrangement may also be employed to execute the sequences of instructions contained in main hard disk memory **807**. In alternative embodiments, hard-wired circuitry may be used in place of or in combination with software instructions. Thus, embodiments are not limited to any specific combination of hardware circuitry and software.

As stated above, the system **801** includes at least one computer readable medium or memory programmed according to the teachings of the invention and for storing data structures, tables, records, or other data described herein. Examples of computer readable media are compact discs, hard disks, floppy disks, tape, magneto-optical disks, PROMs (EPROM, EEPROM, Flash EPROM), DRAM, SRAM, SDRAM, etc. Stored on any one or on a combination of computer readable media, the present invention includes software for controlling the computer system **801**, for driving a device or devices for implementing the invention, and for enabling the computer system **801** to interact with a human user. Such software may include, but is not limited to, device drivers, operating systems, development tools, and applications software. Such computer readable media further includes the

computer program product of the present invention for performing all or a portion (if processing is distributed) of the processing performed in implementing the invention.

The computer code devices of the present invention may be any interpreted or executable code mechanism, including but not limited to scripts, interpreters, dynamic link libraries, Java classes, and complete executable programs. Moreover, parts of the processing of the present invention may be distributed for better performance, reliability, and/or cost.

The term "computer readable medium" as used herein refers to any medium or media that participate in recording data and/or providing instructions to processor **803** for execution. A computer readable medium may take many forms, including but not limited to, non-volatile media, volatile media, and transmission media. Non-volatile media includes, for example, optical, magnetic disks, and magneto-optical disks, such as storage device **807** and/or **808**. Transmission media includes coaxial cables, copper wire and fiber optics, including the wires that comprise bus **802**. Transmission media also may also take the form of acoustic or light waves, such as those generated during radio wave and infrared data communications.

Common forms of computer readable media include, for example, hard disks, floppy disks, tape, magneto-optical disks, PROMs (EPROM, EEPROM, Flash EPROM), DRAM, SRAM, SDRAM, or any other magnetic medium, compact disks (e.g., CD-ROM), or any other optical medium, punch cards, paper tape, or other physical medium with patterns of holes, a carrier wave (described below), or any other medium from which a computer can read.

Various forms of computer readable media may be involved in carrying out one or more sequences of one or more instructions to processor **803** for execution. For example, the instructions may initially be carried on a magnetic disk of a remote computer. The remote computer can load the instructions for implementing all or a portion of the present invention remotely into a dynamic memory and send the instructions over a telephone line using a modem. A modem local to computer system **801** may receive the data on the telephone line and use an infrared transmitter to convert the data to an infrared signal. An infrared detector coupled to bus **802** can receive the data carried in the infrared signal and place the data on bus **802**. Bus **802** carries the data to main hard disk memory **807**, from which processor **803** retrieves and executes the instructions. The instructions received by main hard disk memory

807 may optionally be stored on a removable media storage device **808** either before or after execution by processor **803**.

Computer system **801** also includes a communication interface **813** coupled to bus **802**. Communication interface **813** can be connected to communication port **670** of an internal control/record processor **610**, or internal control/record processor **610** can be eliminated in whole or in part and the communication interface **813** can conduct direct communications with, e.g., level adjuster **630** and gain adjuster **635**. In any such implementation, communication interface **813** sends and receives electrical, electromagnetic, or optical signals that carry data representing various types of information.

Obviously, numerous modifications and variations of the present invention are possible in light of the above teachings. It is therefore to be understood that within the scope of the appended claims, the invention may be practiced otherwise than as specifically described herein.

CLAIMS:

1. An assay device, comprising:
a LED source configured to generate a light;
5 a radial waveguide configured to receive a portion of said light generated by said
LED source and radially distribute said portion of said light;
a plurality of vessel wells each configured to receive an analyte vessel and disposed
radially to said radial waveguide; and
a plurality of light transducers each configured to transduce a transmitted portion of
10 said light radially distributed by said radial waveguide that has passed through said vessel
well.

2. The assay device according to claim 1, further comprising:
a second LED source configured to generate a second light;
15 a second radial waveguide configured to receive a portion of said second light
generated by said second LED source and radially distribute said portion of said second light
to said plurality of vessel wells; and
a second plurality of light transducers each configured to transduce a portion of said
second light radially distributed by said second radial waveguide that has passed through said
20 vessel well.

3. The assay device according to claim 2, wherein said second radial waveguide
comprises a plurality of wedge waveguides.

25 4. The assay device according to claim 1, wherein said radial waveguide comprises a
plurality of wedge waveguides.

5. The assay device according to claim 4, wherein each of said plurality of wedge
waveguides comprises a curved wedge waveguide.

30 6. The assay device according to claim 4, wherein each of said plurality of wedge

waveguides comprises a lensmatic wedge waveguide.

7. The assay device according to claim 1, further comprising a second plurality of light transducers each configured to transduce a portion of said light radially distributed by said radial waveguide that has passed through said vessel well.

8. The assay device according to claim 7, wherein said second plurality of light transducers transduces light that has passed through a side portion of said vessel well.

9. The assay device according to claim 7, wherein said second plurality of light transducers transduces light that has passed through a bottom portion of said vessel well.

10. The assay device according to claim 7, wherein said second plurality of light transducers is used to detect a presence of said analyte vessel in said vessel well.

11. The assay device according to claim 1, further comprising a modulator configured to modulate an intensity of said light generated by said LED source.

12. The assay device according to claim 11, wherein said modulator is configured to turn on and off said LED source.

13. The assay device according to claim 1, wherein said LED source generates light having a wavelength of 470 nm +/- 30 nm.

14. The assay device according to claim 1, further comprising an optical filter.

15. The assay device according to claim 14, wherein said optical filter is disposed along an optical path between said LED source and said radial waveguide

16. The assay device according to claim 1, wherein said plurality of vessel wells is disposed in a substantially circular geometry around said LED source.

17. The assay device according to claim 1, wherein said plurality of vessel wells comprises two concentric circular rows of said vessel wells around said LED source, wherein vessel wells of said two concentric circular rows are staggered to receive said light radially distributed by said radial waveguide.

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18. The assay device according to claim 1, further comprising a plurality of light pipes configured to reflect and conduct said transmitted portion of said light that has passed through said vessel well to said plurality of light transducers.

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19. The assay device according to claim 18, wherein said plurality of light pipes is configured to reflect and conduct said transmitted portion of said light that has passed through said vessel well downward.

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20. The assay device according to claim 19, wherein said plurality of light transducers are disposed in a single plane.

21. The assay device according to claim 18, further comprising a printed circuit board supporting said plurality of light transducers.

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22. The assay device according to claim 1, further comprising a plurality of printed circuit boards supporting said plurality of light transducers.

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23. The assay device according to claim 1, further comprising a vessel support configured to contain said plurality of vessel wells.

24. The assay device according to claim 23, wherein said vessel support comprises:
a heat conducting portion configured to transmit heat to said analyte vessel in said vessel wells; and

30

a heater configured to maintain said heat conducting portion substantially at an incubation temperature.

25. The assay device according to claim 23, wherein said vessel support further

comprises:

a heat insulating portion configured to thermally insulate said heat conducting portion.

5 26. The assay device according to claim 24, wherein said heater comprises a DC heater.

27. The assay device according to claim 24, wherein:

said heater comprises a ring heater; and

10 said heat conducting portion comprises a heat conducting ring.

28. The assay device according to claim 27, wherein said ring heater is disposed around said heat conducting ring.

15 29. The assay device according to claim 1, further comprising a precalibrated temperature transducer.

30. The assay device according to claim 24, further comprising a precalibrated temperature transducer disposed within said heat conducting portion

20

31. An assay device, comprising:

a light source configured to generate a light;

a plurality of vessel wells each configured to receive an analyte vessel and disposed in an optical path of a portion of said light generated by said light source;

25 a plurality of optical pipes each configured to receive said portion of said light transmitted along a respective of said optical paths through a respective of said plurality of vessel wells and reflect and conduct said received light; and

a single printed circuit board including a plurality of light transducers each configured to transduce a portion of said light reflected and conducted by a respective of said plurality of optical pipes.

30

32. An assay device, comprising:

a light source configured to generate a light;
a plurality of vessel wells each configured to receive an analyte vessel and disposed
in an optical path of a portion of said light generated by said light source;
a plurality of optical pipes each configured to receive said portion of said light
transmitted along a respective of said optical paths through a respective of said plurality of
vessel wells and reflect and conduct said received light downward; and
a printed circuit board disposed below said plurality of vessel wells and including a
light transducer configured to transduce a portion of said light reflected and conducted by a
respective of said plurality of optical pipes.

33. An assay device, comprising:
a vessel support configured to contain said plurality of vessel wells each configured
to receive an analyte vessel, said vessel support including
a heat conducting portion configured to transmit heat to said analyte vessel in said
vessel wells,
a heat insulating portion configured to thermally insulate said heat conducting
portion, and
a heater configured to maintain said heat conducting portion substantially at an
incubation temperature.

34. The assay device according to claim 33, wherein:
said heater comprises a ring heater; and
said heat conducting portion comprises a heat conducting ring.

35. The assay device according to claim 34, wherein said ring heater is disposed
around said heat conducting ring.

36. A method for performing assays comprising:
generating light using a LED;
radially guiding a portion of the generated light;
transmitting a portion of the guided light through a plurality of vessels; and
transducing a portion of the transmitted light to perform an assay.

37. The method according to claim 36, wherein said transmitting step further comprises transmitting a second portion of said guided light through one of a side and a bottom portion of said plurality of vessels to detect the presence of said plurality of vessels.

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38. The method according to claim 36, further comprising reflecting said transmitted light from a plurality of vessels in a same direction.

39. The method according to claim 36, further comprising diverging said portion of said generated light.

10

40. The method according to claim 39, wherein said diverging step and said radially guiding step are performed by a same light guide.

15

41. The method according to claim 36, further comprising modulating an intensity of said portion of the transmitted light.

42. The method according to claim 41, wherein said modulating step comprises modulating a generated light intensity.

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43. The method according to claim 41, wherein said modulating step comprises alternatively starting and stopping said generating of light.

44. The method according to claim 41, further comprising correcting for a background light intensity.

25

45. A device for performing assays, comprising:

means for generating light;

means for radially guiding a portion of the generated light;

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means for transmitting a portion of the guided light through a plurality of vessels; and

means for transducing a portion of the transmitted light to perform an assay.

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46. An assay device, comprising:
a LED source configured to generate a light;
radial waveguide means for receiving a portion of said light generated by said LED
source and radially distribute said portion of said light;
5 a plurality of vessel wells each configured to receive an analyte vessel and disposed
radially to said radial waveguide means; and
a plurality of light transducer means for transducing a transmitted portion of said light
radially distributed by said radial waveguide means that has passed through said vessel well.

10 47. The assay device according to claim 46, further comprising:
a second LED source configured to generate a second light;
second radial waveguide means for receiving a portion of said second light generated
by said second LED source and radially distribute said portion of said second light to said
plurality of vessel wells; and
15 a second plurality of light transducer means for transducing a portion of said second
light radially distributed by said second radial waveguide means that has passed through said
vessel well.

20 48. The assay device according to claim 47, wherein said second radial waveguide
means comprises a plurality of wedge waveguide means.

49. The assay device according to claim 47, wherein said radial waveguide means
comprises a plurality of wedge waveguide means.

25 50. The assay device according to claim 49, wherein each of said plurality of wedge
waveguide means comprise a curved wedge waveguide.

51. The assay device according to claim 49, wherein each of said plurality of wedge
waveguide means comprises a lensmatic wedge waveguide means.

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52. The assay device according to claim 46, further comprising a second plurality of light transducer means for transducing a portion of said light radially distributed by said radial waveguide means that has passed through said vessel well.

5 53. The assay device according to claim 52, wherein said second plurality of light transducer means transduces light that has passed through a side portion of said vessel well.

10 54. The assay device according to claim 52, wherein said second plurality of light transducer means transduces light that has passed through a bottom portion of said vessel well.

15 55. The assay device according to claim 52, wherein said second plurality of light transducer means comprises transducer means for detecting a presence of said analyte vessel in said vessel well.

56. The assay device according to claim 46, further comprising a means for modulating an intensity of said light generated by said LED source.

20 57. The assay device according to claim 56, wherein said means for modulating comprised a means for turning on and off said LED source.

58. The assay device according to claim 46, wherein said LED source generates light having a wavelength of 470 nm +/- 30 nm.

25 59. The assay device according to claim 46, further comprising a means for filtering a light.

30 60. The assay device according to claim 59, wherein said means for filtering is disposed along an optical path between said LED source and said radial waveguide means.

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61. The assay device according to claim 46, wherein said plurality of vessel wells are disposed in a substantially circular geometry around said LED source.

62. The assay device according to claim 46, wherein said plurality of vessel wells comprises two concentric circular rows of said vessel wells around said LED source, wherein vessel wells of said two concentric circular rows are staggered to receive said light radially distributed by said radial waveguide.

63. The assay device according to claim 46, further comprising a plurality of means for reflecting and conducting said transmitted portion of said light that has passed through said vessel well to said plurality of light transducer means.

64. The assay device according to claim 63, wherein said means for reflecting and conducting are configured to reflect said transmitted portion of said light that has passed through said vessel well downward.

65. The assay device according to claim 64, wherein said plurality of light transducer means are disposed in a single plane.

66. The assay device according to claim 63, further comprising a means for supporting said plurality of light transducers.

67. The assay device according to claim 46, further comprising a plurality of means for supporting said plurality of light transducers.

68. The assay device according to claim 46, further comprising a means for supporting said plurality of vessel wells.

69. The assay device according to claim 68, wherein said means for supporting comprises:

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means for conducting heat to said analyte vessel in said vessel wells; and
means for maintaining said means for conducting substantially at an incubation
temperature.

5 70. The assay device according to claim 68, wherein said vessel support further
comprises:

means for thermally insulating said means for conducting.

10 71. The assay device according to claim 69, wherein said means for maintaining
comprises a DC means for maintaining.

15 72. The assay device according to claim 69, wherein:
said means for maintaining comprises an annular means for maintaining; and
said means for conducting comprises an annular means for conducting.

 73. The assay device according to claim 72, wherein said annular means for
maintaining is disposed around said annular means for conducting.

20 74. The assay device according to claim 46, further comprising a precalibrated
means for transducing temperature.

 75. The assay device according to claim 69, further comprising a precalibrated
means for transducing temperature disposed within said means for conducting.

25 76. An assay device, comprising:
means for generating a light;
plural means for receiving an analyte vessel, each disposed along an optical path of a
portion of said light generated by said light generating means;
a plurality of means for redirecting light, each configured to receive said portion of
30 said light transmitted along a respective of said optical paths through a respective of said

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plurality of means for receiving; and

a single means for supporting a plurality of means for transducing a portion of said light reflected by said plurality of means for redirecting light.

5 77. An assay device, comprising:

means for generating a light;

plural means for receiving an analyte vessel, each disposed along an optical path of a portion of said light generated by said light generating means;

10 a plurality of means for redirecting light downward, each configured to receive said portion of said light transmitted along a respective of said optical paths through a respective of said plurality of means for receiving; and

a means for transducing a portion of said light reflected downward by said plurality of means for redirecting light.

15 78. An assay device, comprising:

means for receiving an analyte vessel, said means for receiving including

means for conducting heat to said analyte vessel in said means for receiving,

means for thermally insulating said means for conducting heat, and

means for maintaining said means for conducting heat substantially at an incubation

20 temperature.

79. The assay device according to claim 78, wherein:

said means for maintaining comprises an annular means for maintaining; and

said means for conducting heat comprises an annular means for conducting heat.

25 80. The assay device according to claim 79, wherein said annular means for maintaining is disposed around said annular means for conducting heat.

81. The assay device according to claim 1, wherein said LED source generates light
30 having a wavelength of 430 nm +/- 30 nm.

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82. The assay device according to claim 1, wherein said LED source generates light having a wavelength less than 720 nm.

83. The assay device according to claim 11, wherein said modulator comprises a
5 control processor.

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PYROS KINETIX READER FOR CONDUCTING ASSAYS

5

ABSTRACT OF THE DISCLOSURE

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An analytical device that can be used to conveniently and accurately assay plural vessels. In one exemplary embodiment, a pair of LED sources provides illumination through a pair of radial waveguides to plural vessels arranged in a pair of substantially concentric and circular rows about the LED sources. A light pipe receives light transmitted through a vessel from each radial waveguide and reflects the received light downward to a single printed circuit board that contains a photodiode for each light pipe, as well as processing circuitry. The first LED source/radial waveguide optical is used to confirm the presence of a vessel, and the second is used to perform, e.g., turbidometric and/or colorimetric assays upon an

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analyte within the vessel. The vessel is incubated in a vessel support that includes a heat conducting base and a heat insulating cover. Heat is supplied by a DC heater.

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FIG. 1A

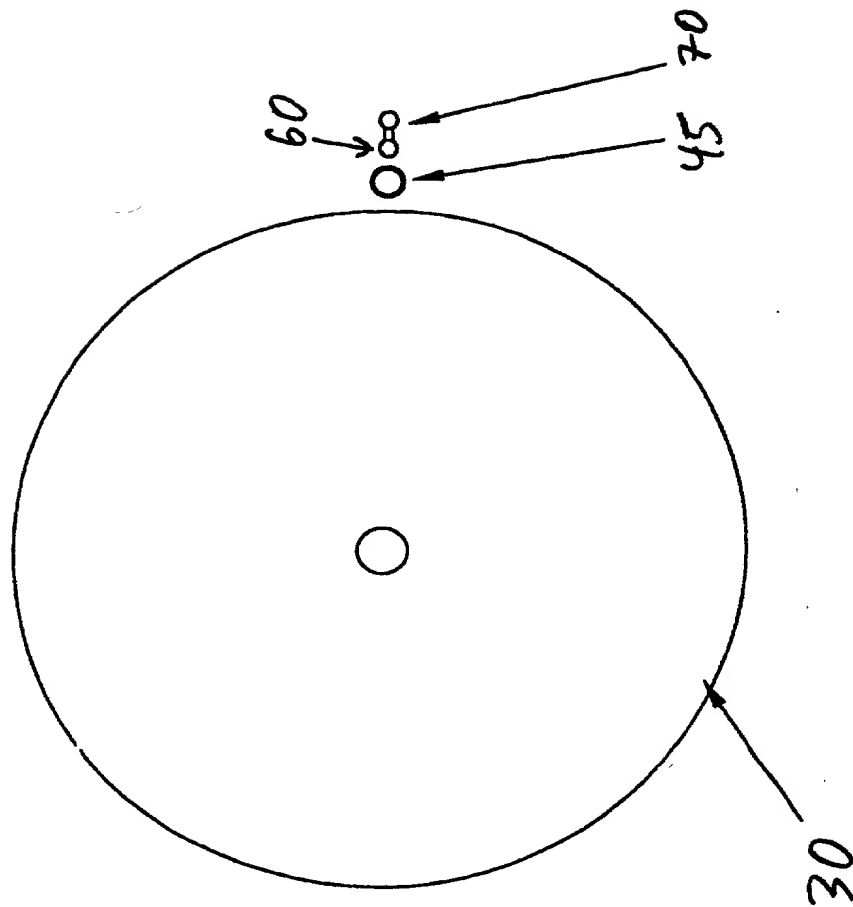
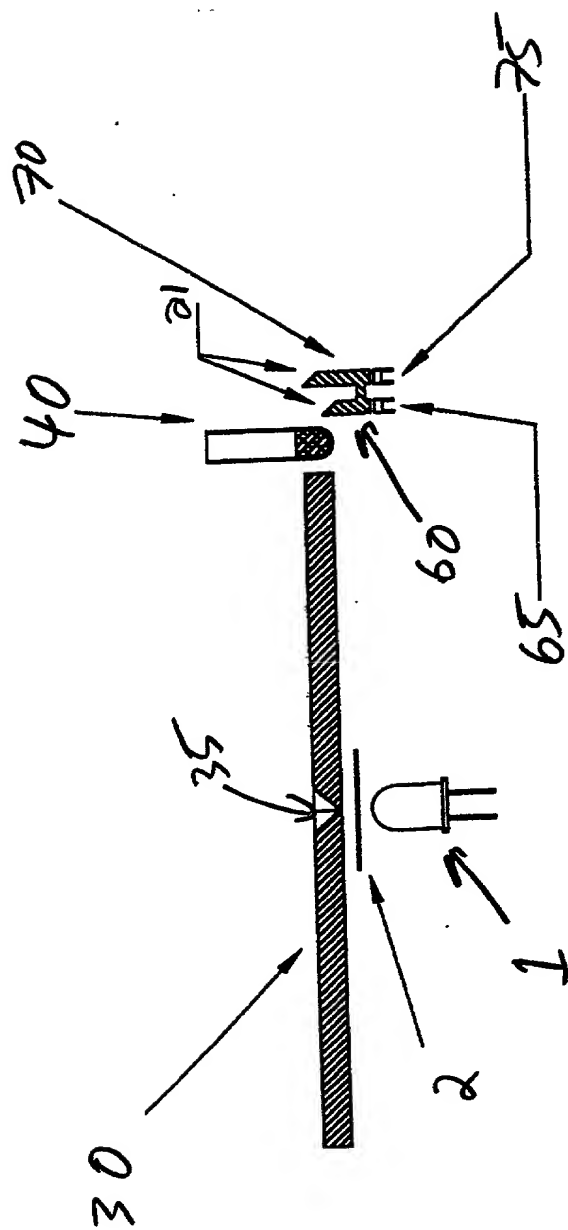


FIG. 10



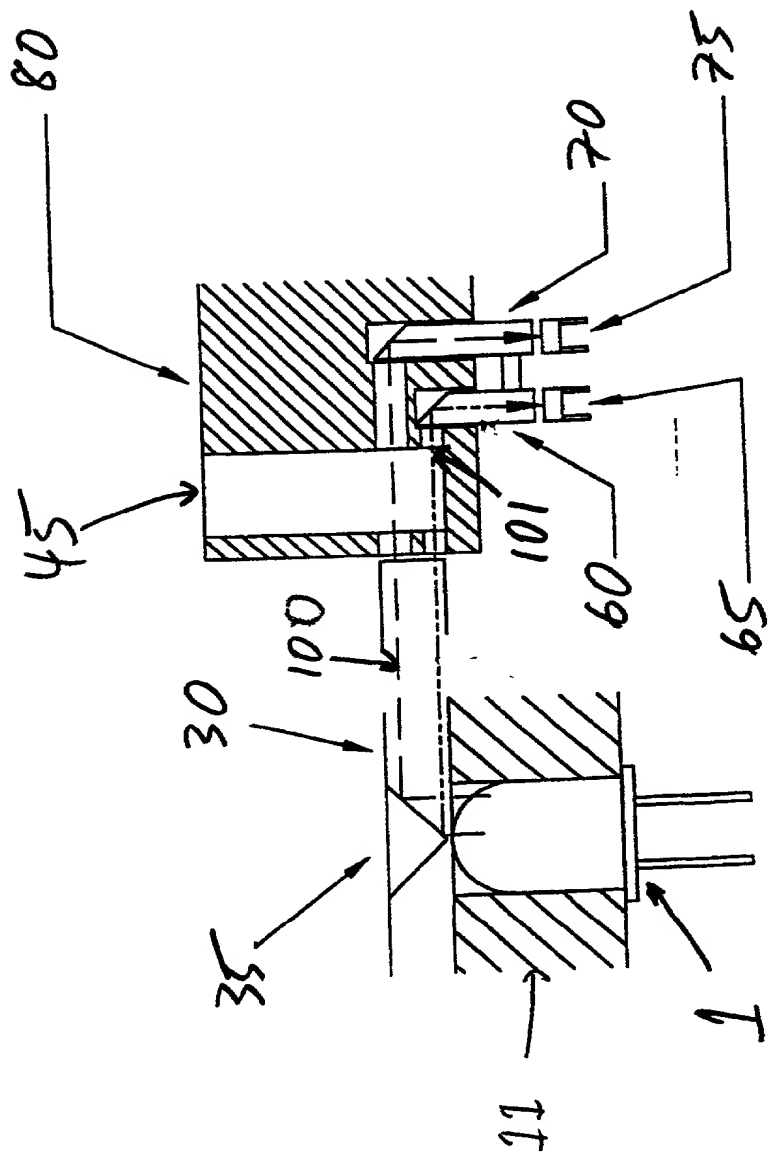


FIG. 2A

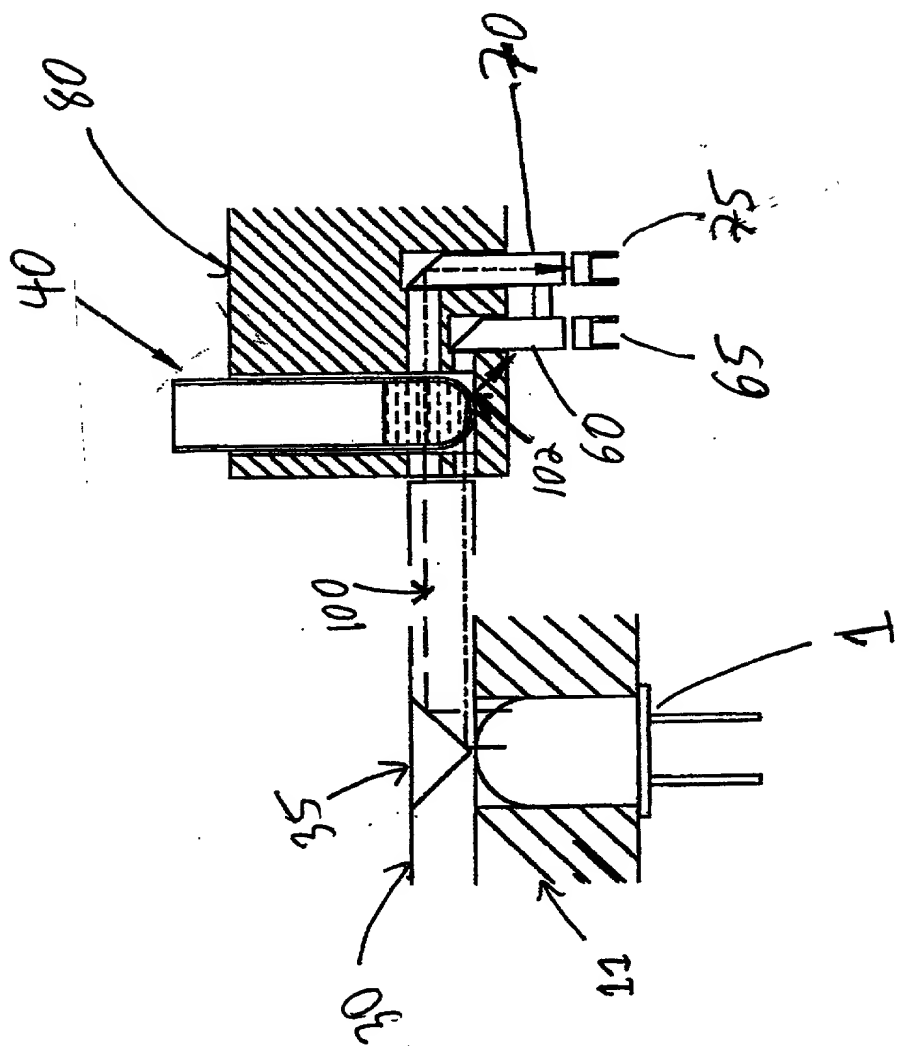


FIG. 2B

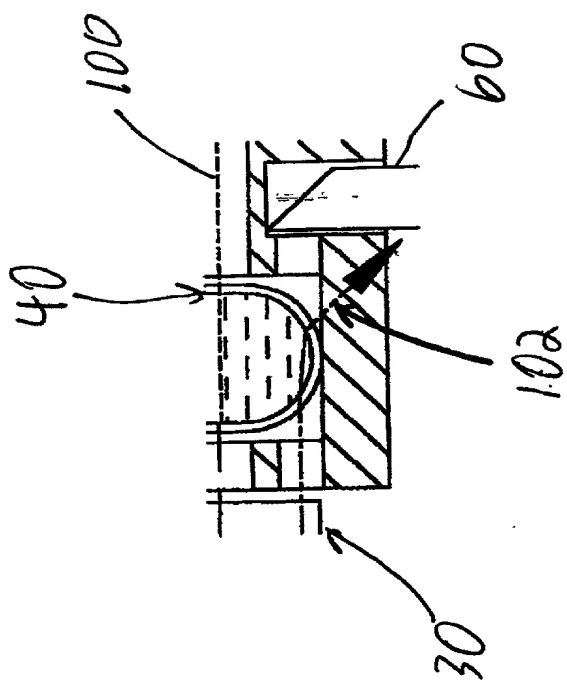


FIG. 2C

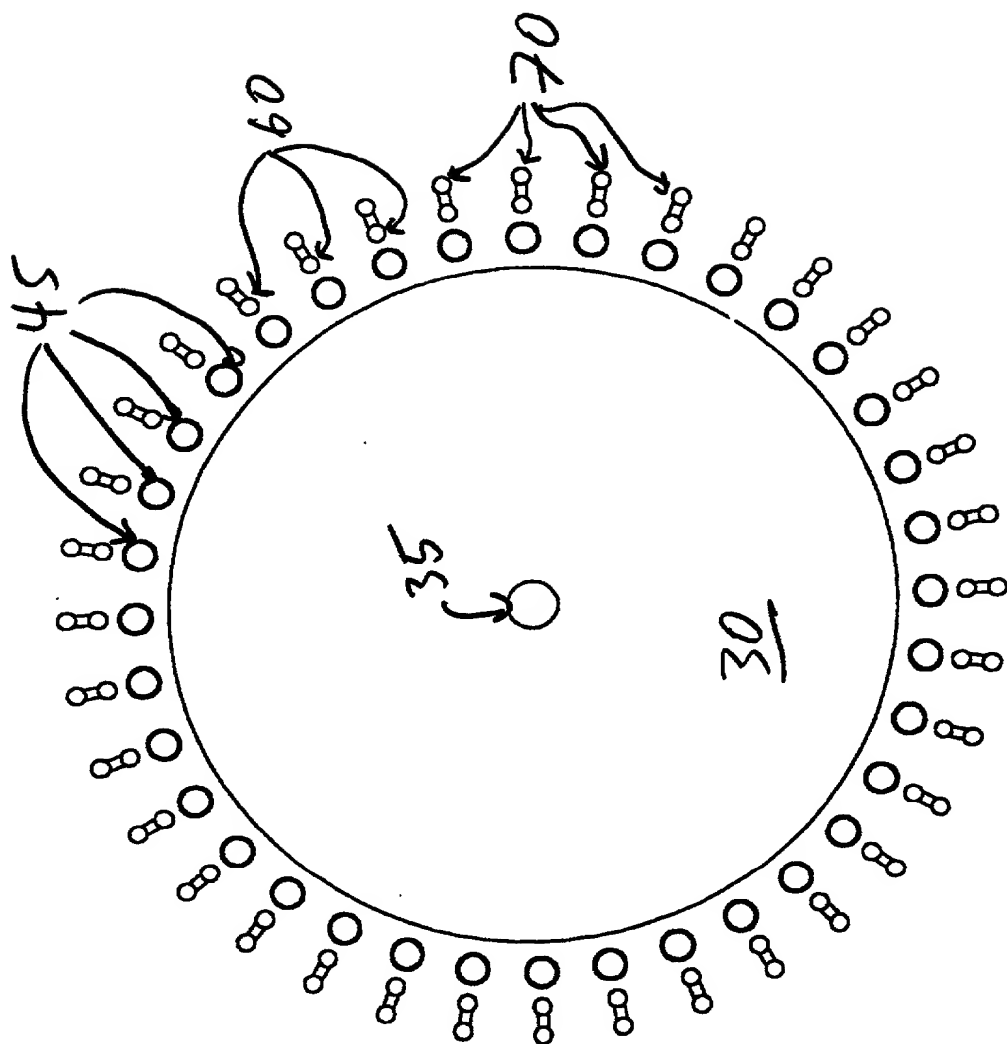
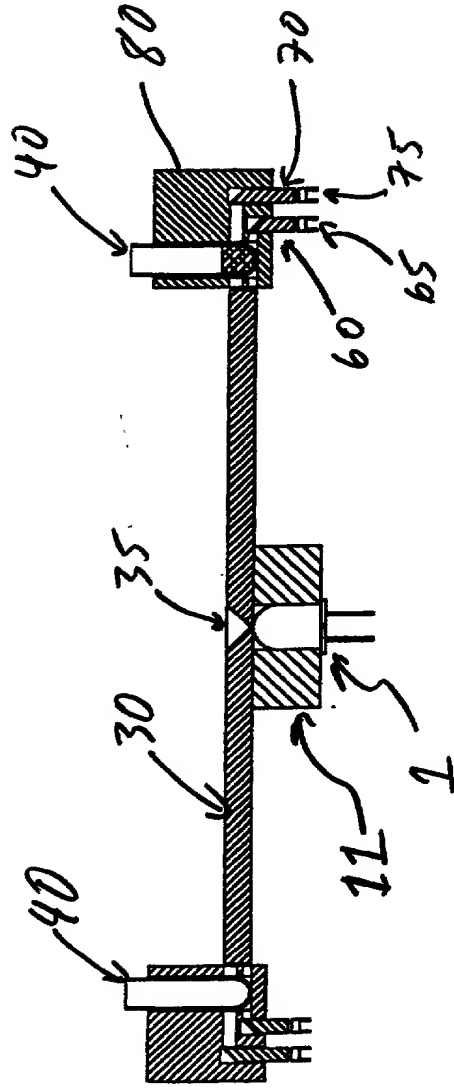


FIG. 3A



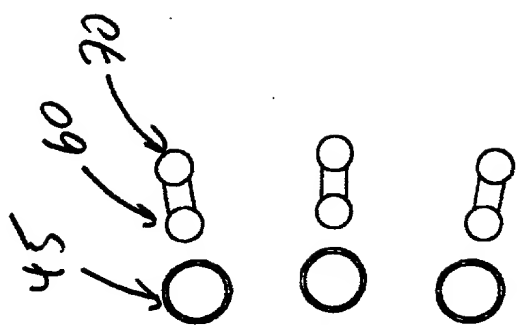


FIG. 4A

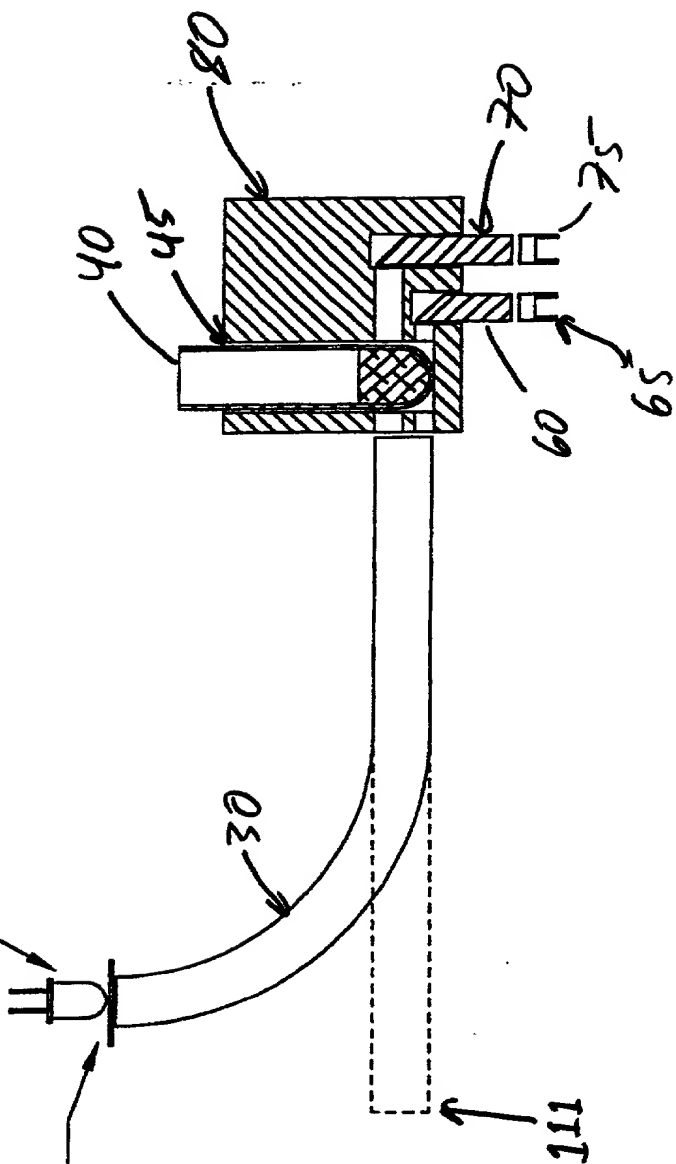


FIG. 4B

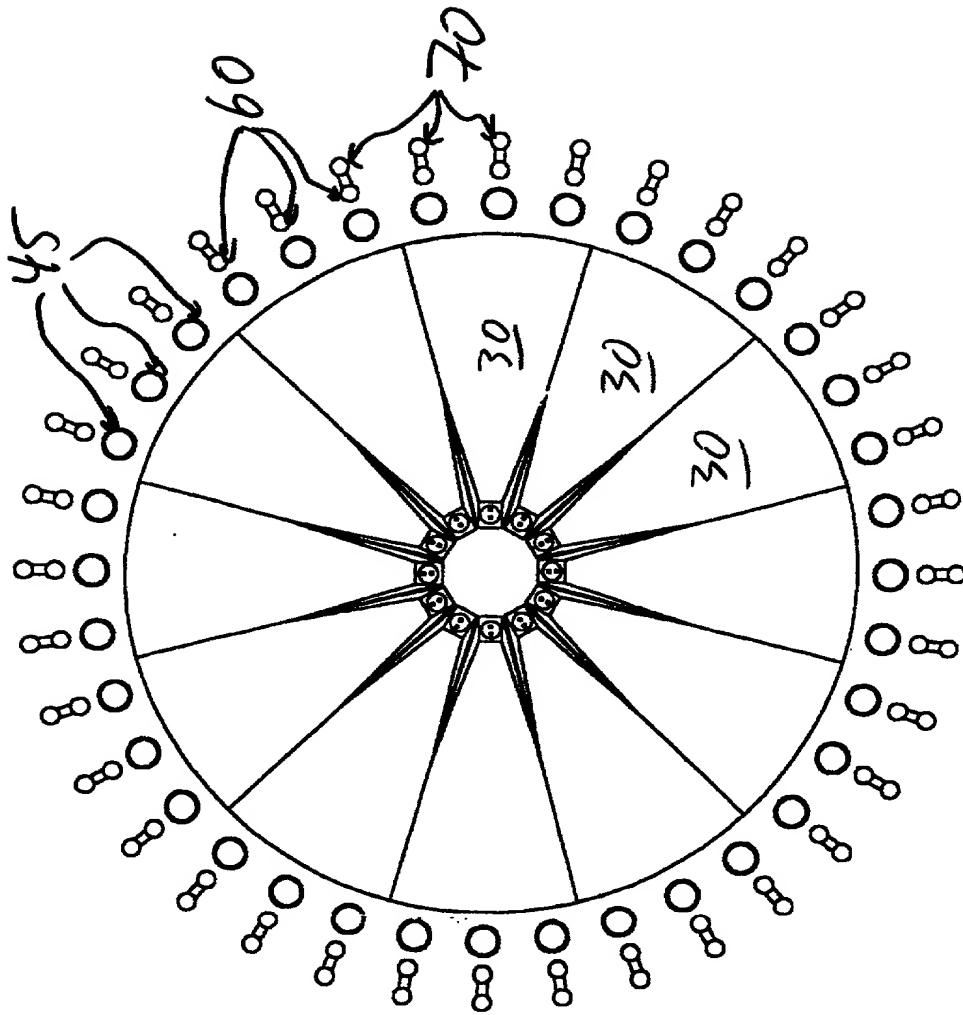


FIG. 5A

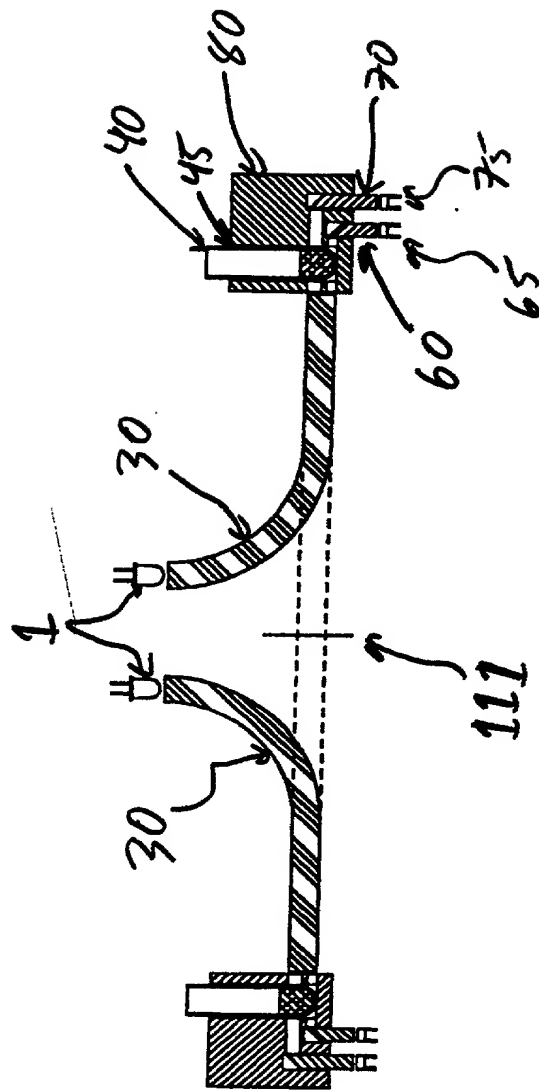
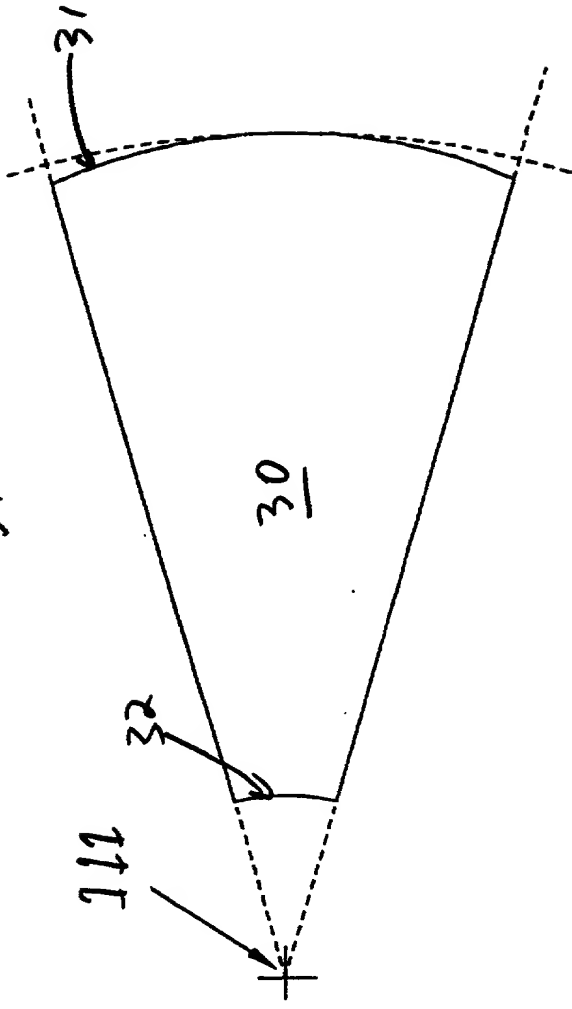
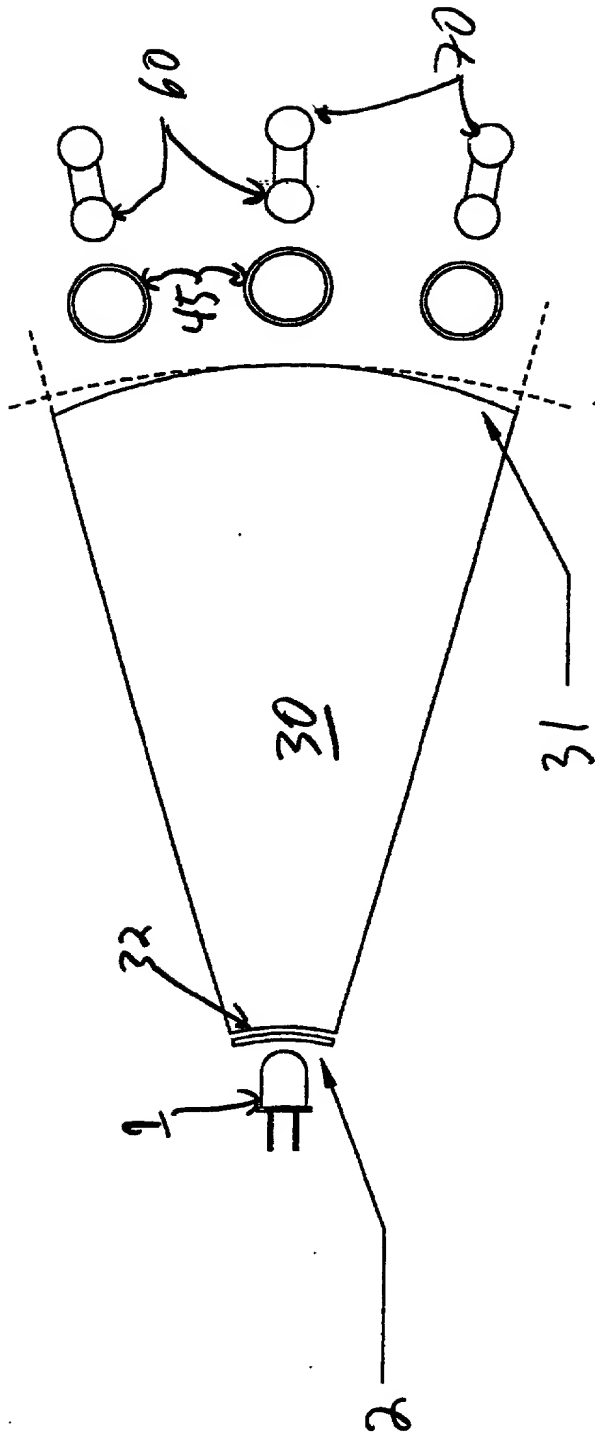


Fig. 50



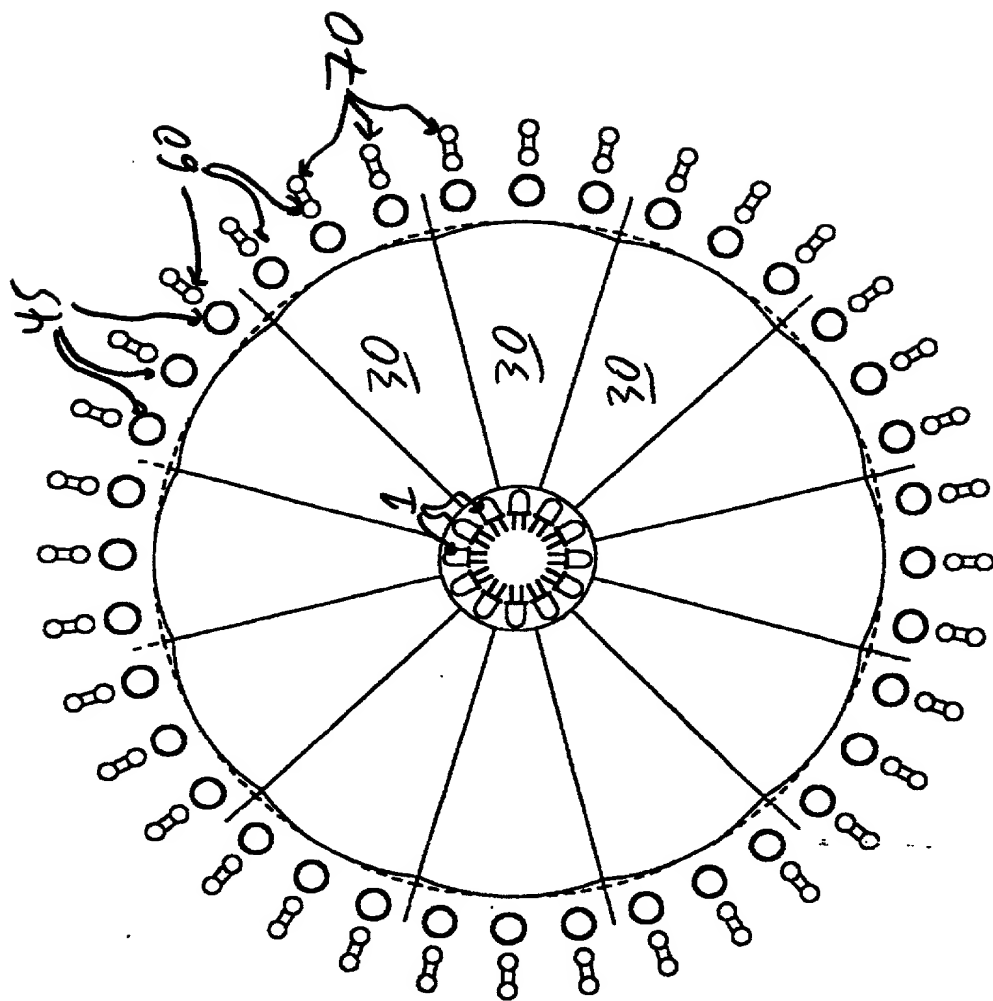


FIG. 7A

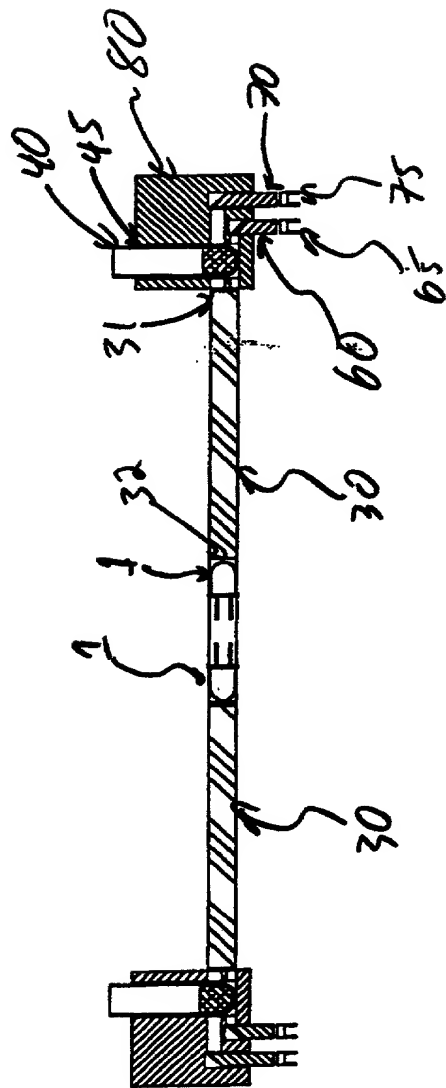


FIG. 70

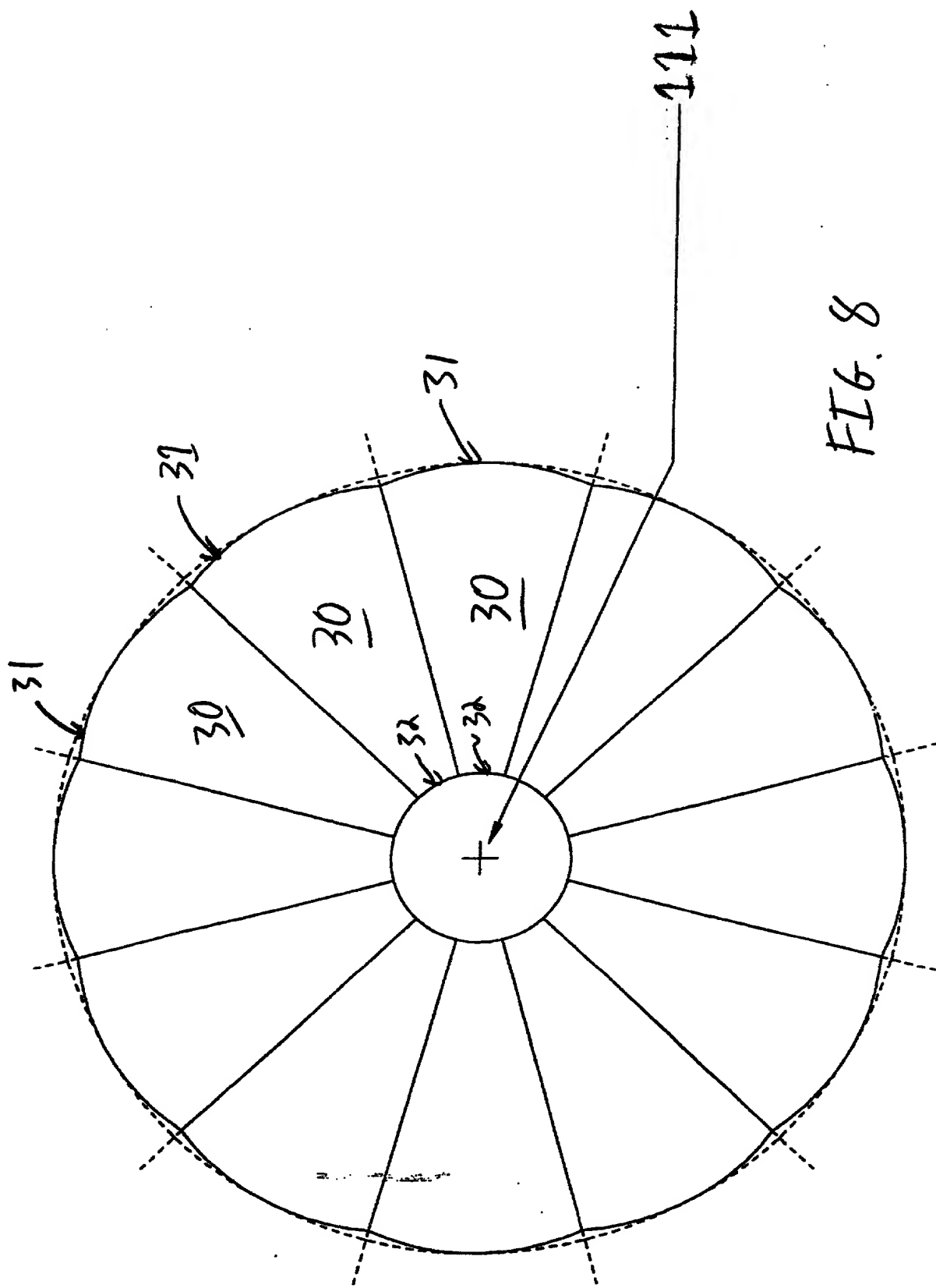


FIG. 8

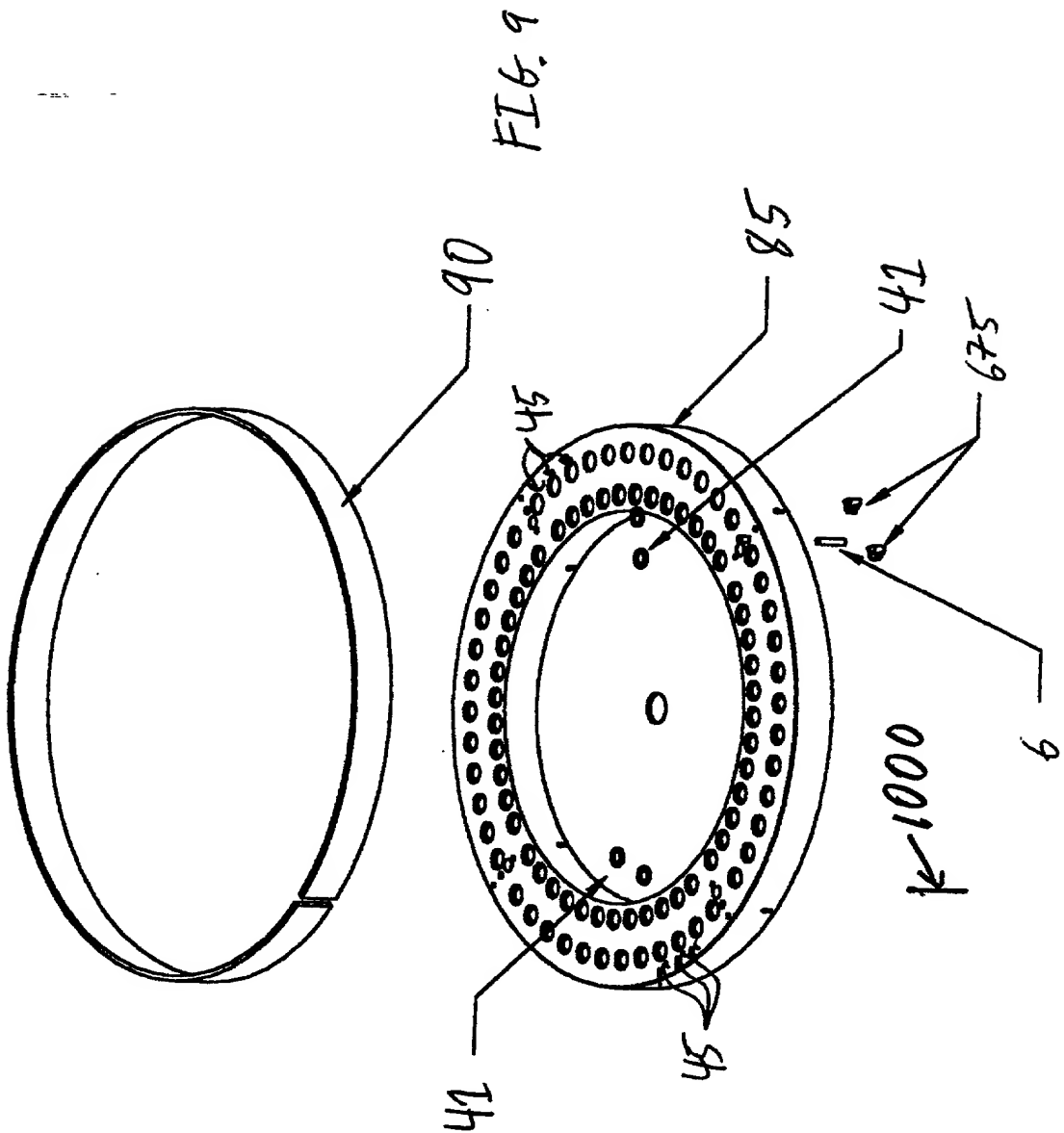
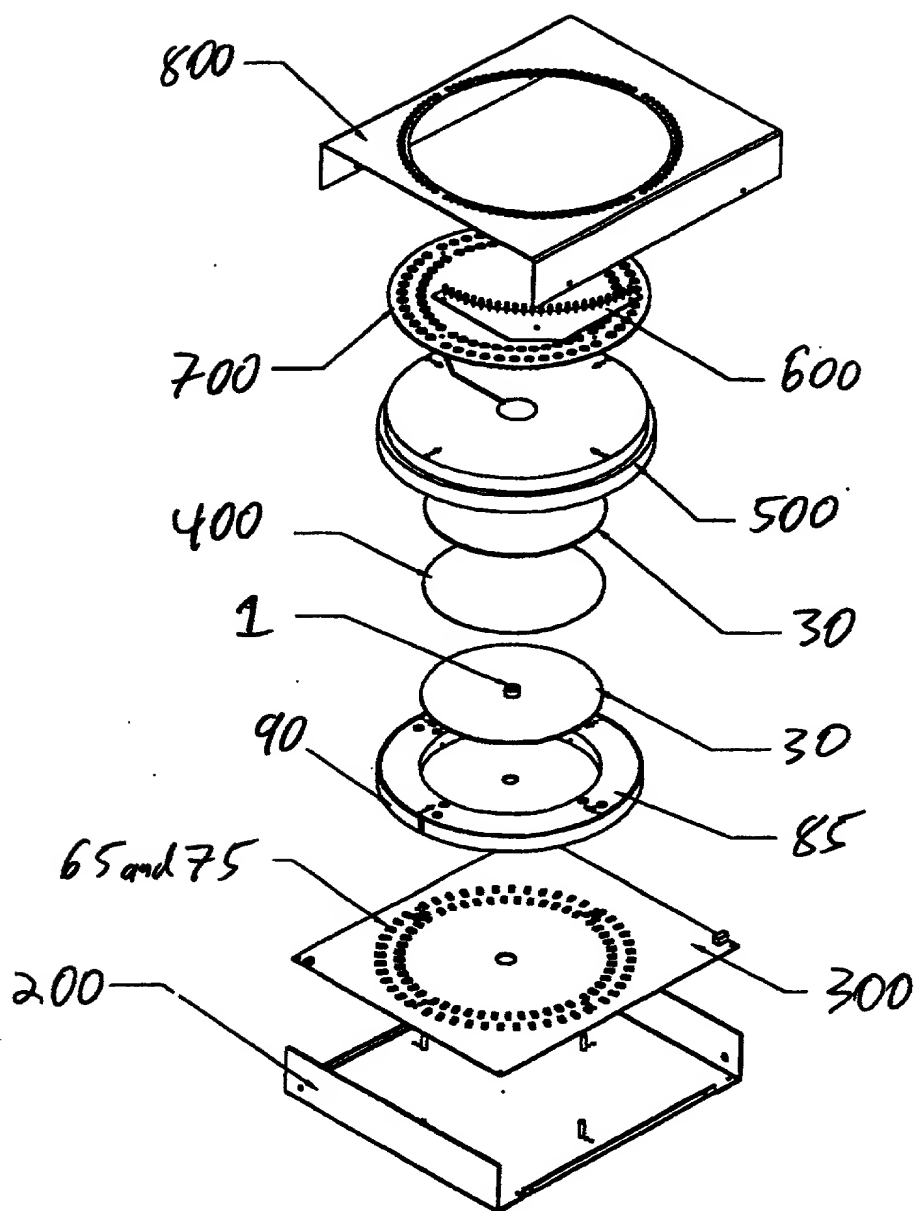


FIG. 10



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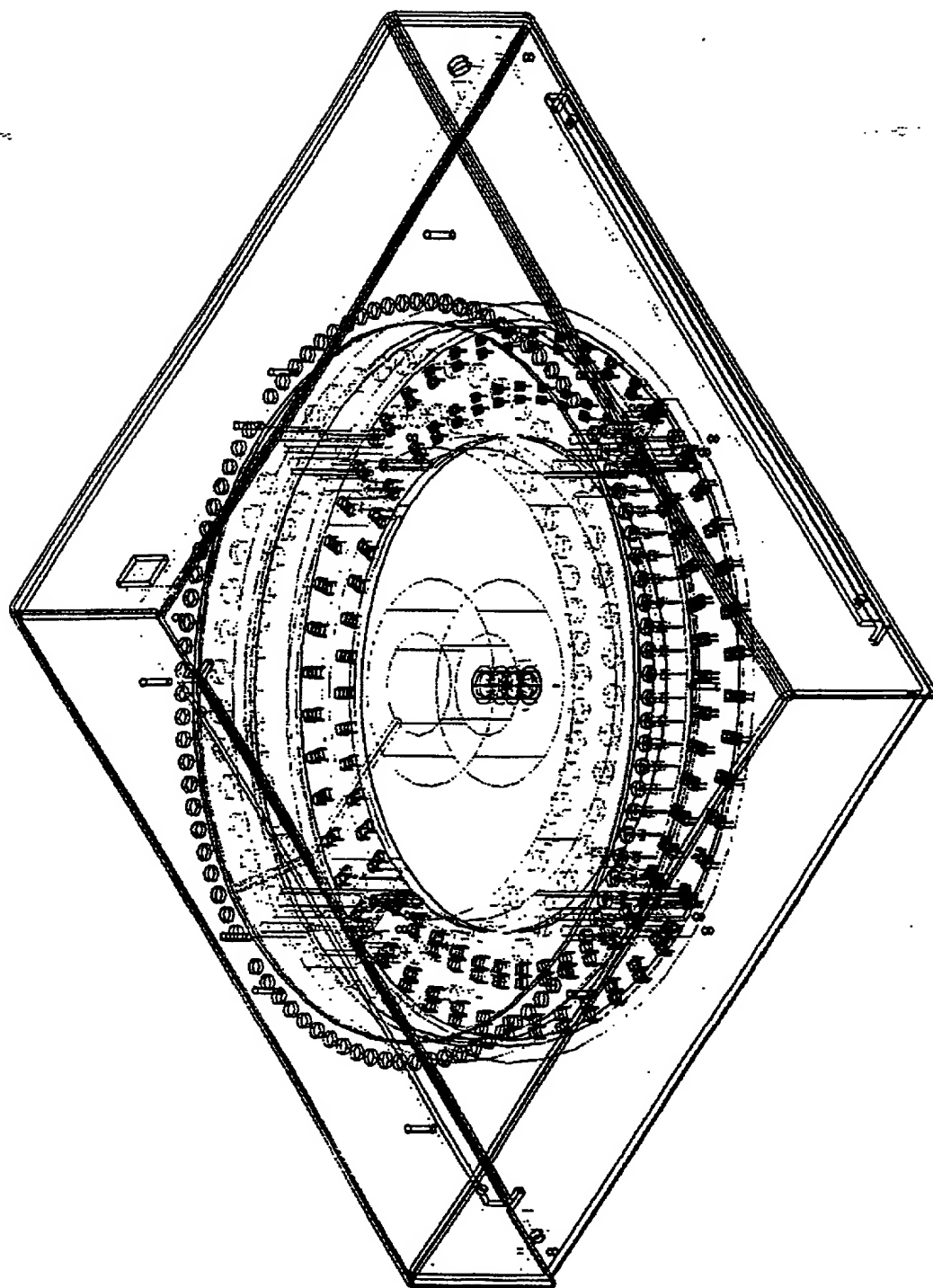
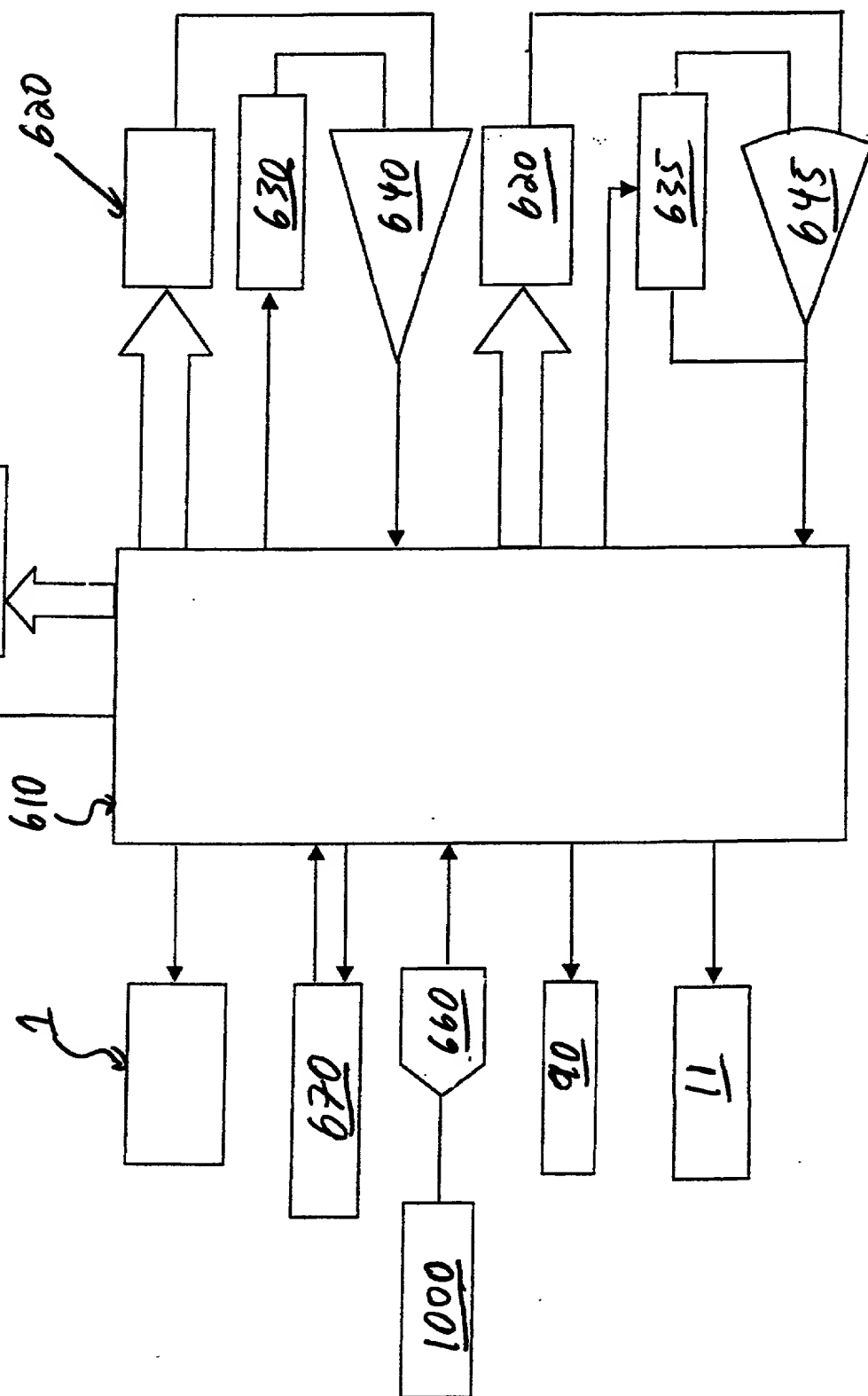


FIG. 11

FIG. 12



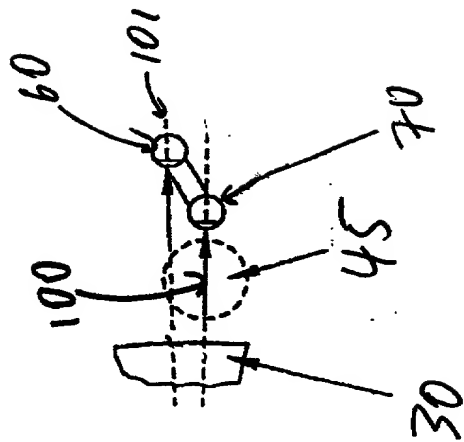


FIG. 13A

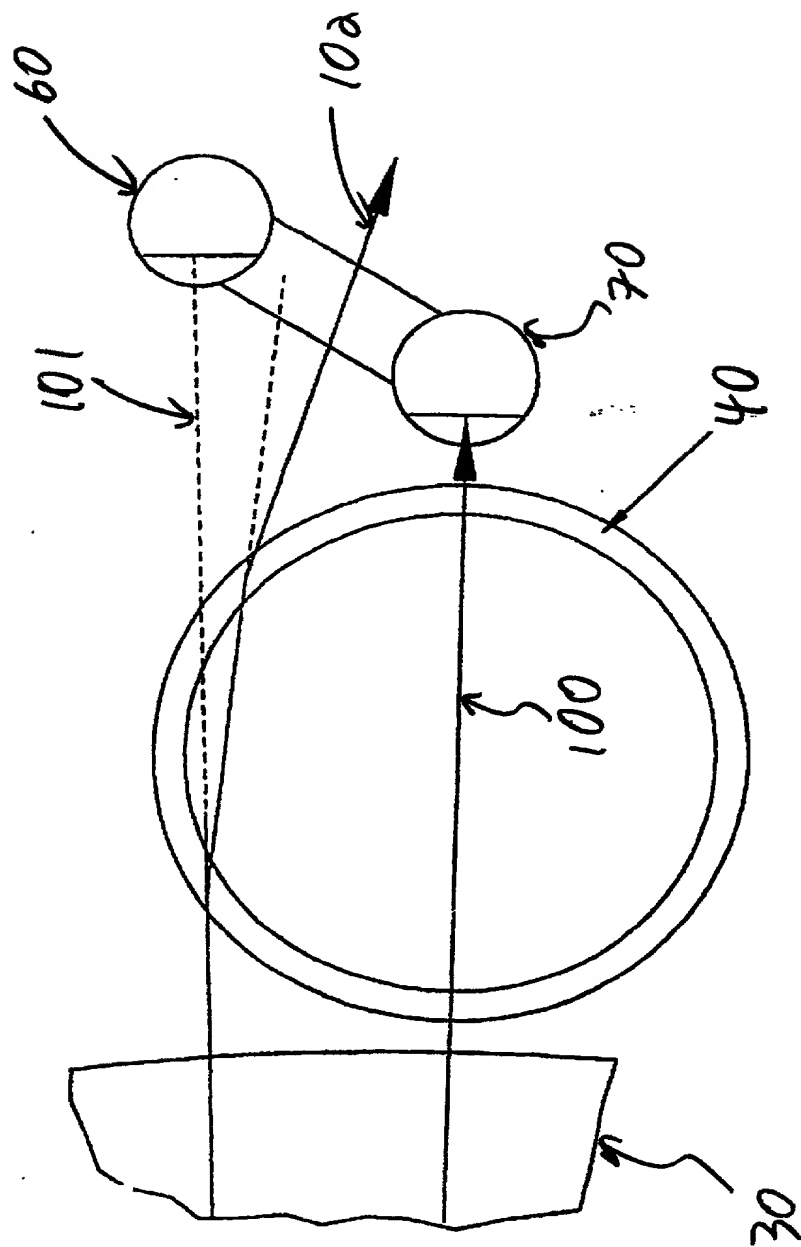


FIG. 130

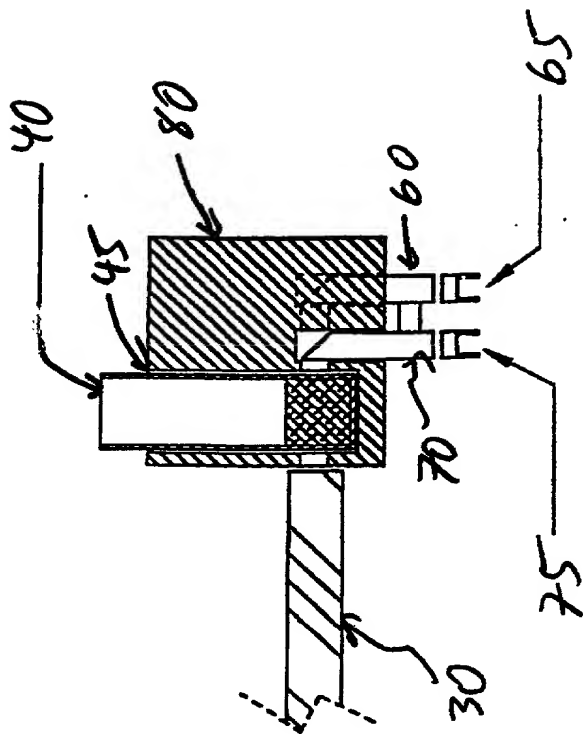


FIG. 13C

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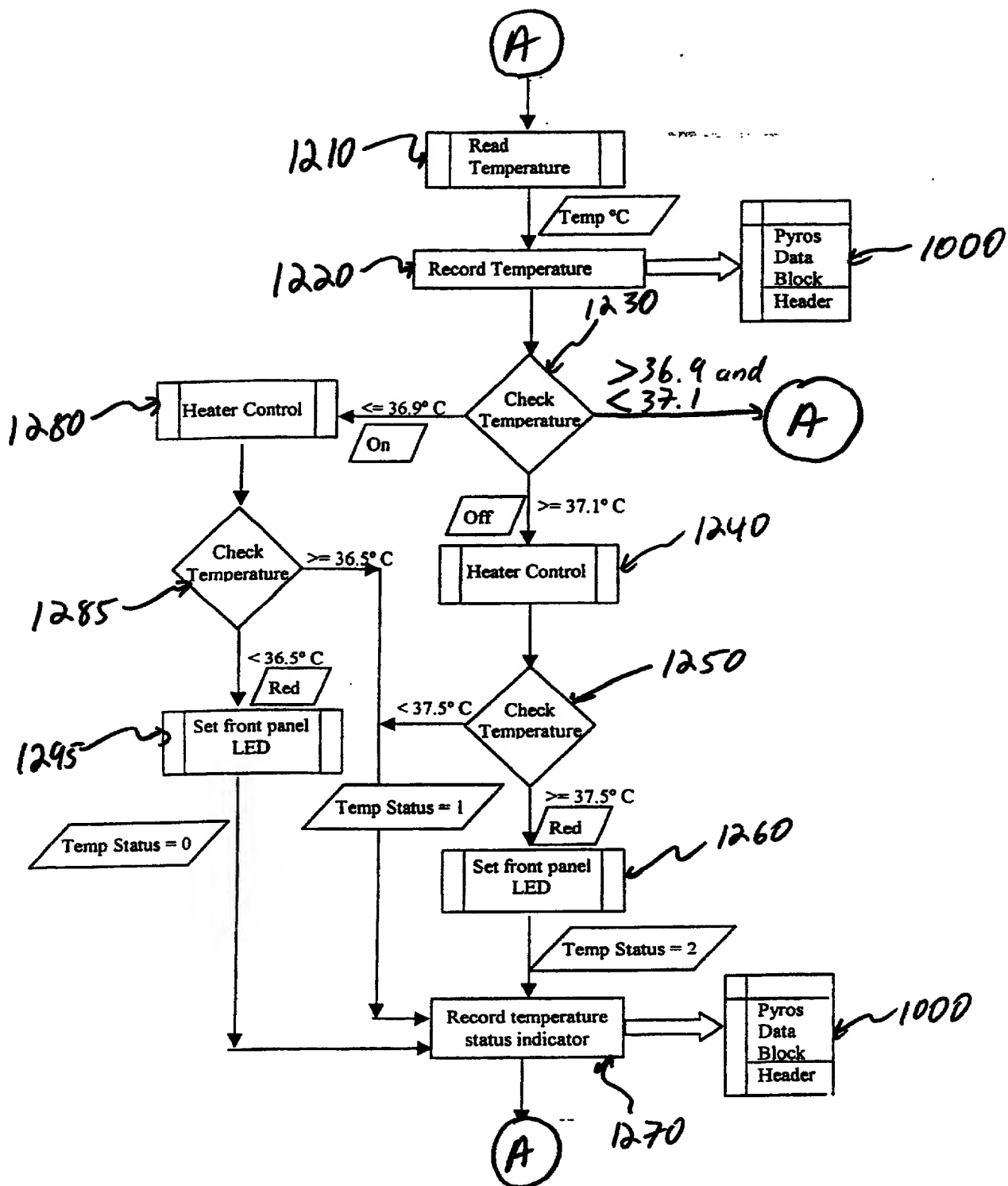


FIG. 14

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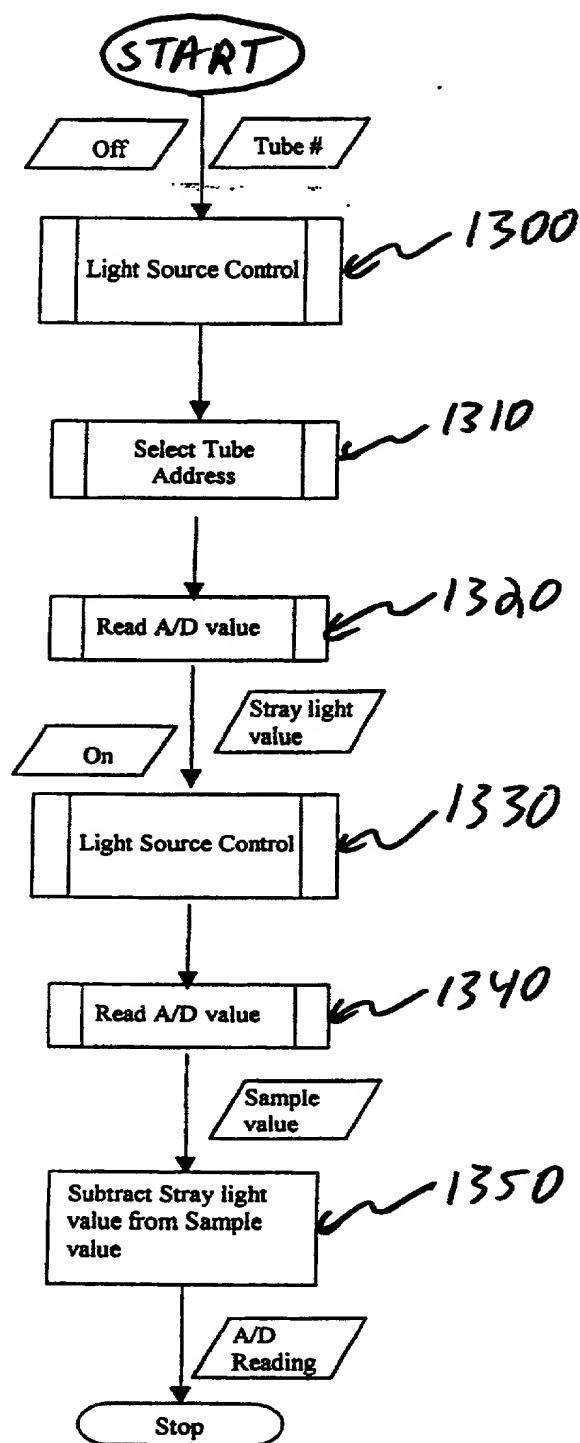


FIG. 15

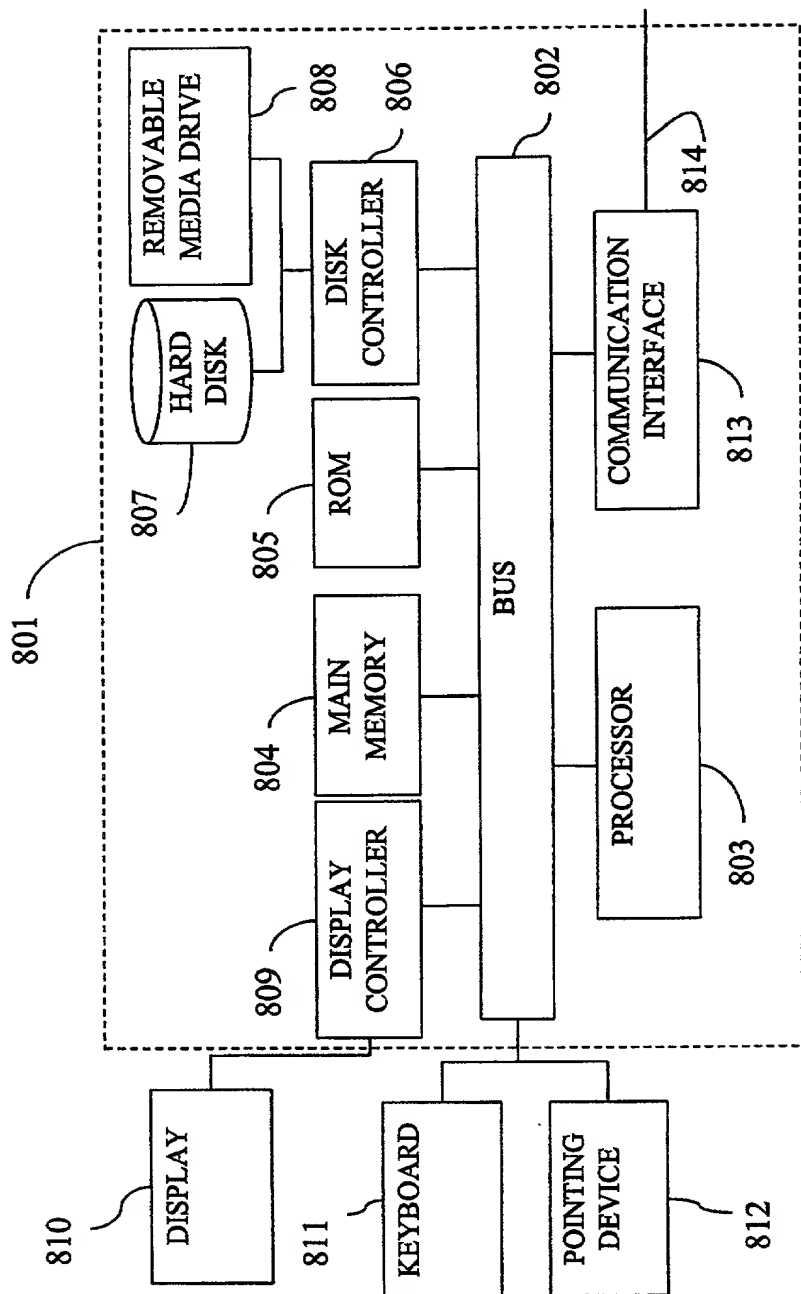


FIG. 16